



Analysis of OCR and DFR Relay Coordination on Transmission Lines

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ABSTRACT—

The electrical energy landscape undergoes continuous transformations throughout the years, with a growing inclination towards renewable energy sources as opposed to traditional thermal power generation facilities. The current generations are driven by the desire for access to high-quality power while taking into account economic factors. The primary purpose of the protection system is to promptly detect and separate the faulty sections from the functional sections of power systems within a certain timeframe, in order to prevent significant disruptions in power supply. Electrical power systems are susceptible to a range of symmetrical and unsymmetrical errors, as well as short circuits. Transformer protection is achieved through the utilization of protective relays, namely OCR and GFR. The proposed testing system is deployed on the ETAP platform and the outcomes are assessed. The Time Multiplier Setting (TMS) calculations are derived from the plots of Time Current Characteristics.

Keywords— Over Current Relay, Differential Relay, Wind power system, ETAP, Short Circuit Analysis, Load Flow Analysis

I. INTRODUCTION

Any electricity network needs protective relays to quickly deactivate faulty components to prevent system interruption and maintain network efficiency. After primary relay functionality stops, backup relays take over. The protective relay should distinguish normal, abnormal, and fault conditions.^[1] Relay coordination involves identifying, selecting, and protecting against threats. Economically expanding nations use power more. Electrical firms use more complex networks. In order to ascertain the minimum margin of divergence of a relay and the back-up relays in an intricate electrical system, it is necessary to conduct a load flow evaluation, fault calculations, and compile a list of primary and stand by pairs.^[2-4] It will also take several TMS calculation iterations. Only computer programming can do this. The ETAP load schedule program can monitor and report voltage and short-circuit current for 10,000,000 load items. In addition to 10,000,000 load items, it can manage 1000 buses. Due to rising load demand, power system designers and operators worldwide are concerned about system reliability and efficacy. Since its penetration has increased, Distributed Generation

(DG) in Distribution systems can now cover most load needs. DG units affect voltage stability, frequency deviation, and relay coordination, thus they must be carefully examined.^[5] This work introduces a new relay coordination approach for wind turbine generator dependability evaluation. Change the pick-up value, PSM, and TDS to synchronize visually and physically. Further reliability testing is done

II. RENEWABLE POWER

A. Wind Power Forecasting

The system under consideration encompasses Wind Energy Conversion Systems (WECS), Diesel generators, and Solar generators. The performance study on ETAP load flow and short circuit analysis has been conducted. The assessment of relay coordination for different faults has been conducted, along with an examination of the behavior of distributed generators (DGs) during faults. This study provides a comprehensive analysis of the proposed test system across several operational scenarios including the aforementioned kinds of distributed generators (DGs).^[15]

III. PROPOSED METHODOLOGY

- A. **Effect of WT Generation System on RC** Digital grid (DG) systems distribute the load at their point of contact inside the electrical grid. The load can be handled by both islanding and non-islanding diesel generators. Distributed generation (DG) has the potential to induce fault current, so altering the amplitude and direction of the power flow, often characterized by uni-directionality. Every energy grid zone encompasses at least one aspect and aims to decrease the time required to clear faults.[16,17] The investigation of relay qualities involves the analysis of time current characteristic curves. The min and max curves of the relay are modified by TDS. Primary and backup protection are

the two forms of protection that are offered. Backup security is the subsequent layer of protection that follows primary security measures. Backup security must exhibit greater resilience to faults compared to primary security, and it should also have a longer lifespan. The coordination time interval (CTI) refers to the temporal disparity between the tripping times of the primary and secondary relays. Typically, the duration ranges from 0.2 to 0.5 seconds. [18] Proposed System has been shown below in Fig. 1 developed on ETAP.

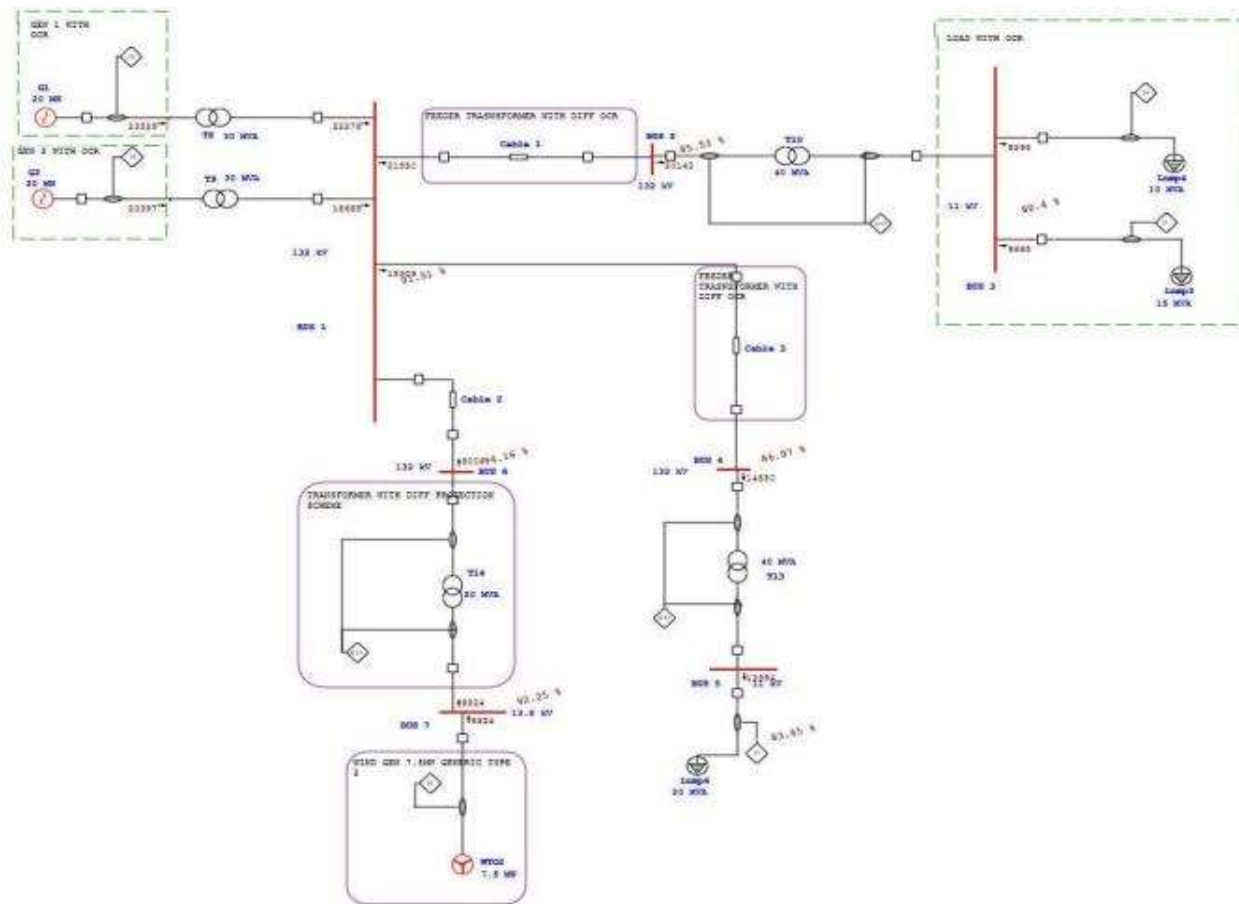


Figure 1: RES Integrated Network

B. Load Flow Analysis The proposed system underwent a LFA utilizing the ANRI method with 99 iterations and $10e4$ accuracy.^[19-20] Power flow at each bus is shown in the fig 3 for the overall system and the WTG linked bus. Fig 1 shows the LFA study case editor to illustrate the approach. The LFA with 0 MW power discrepancy reports, bus loading, branches, branch losses, bus inputs, cables, transformers, generations, and others.^[21]

C. Short Circuit Analysis

When used, electrical system and computer networks often malfunction. The network's devices' internal electromotive forces and system and network impedances control current flow during a malfunction. However, computer reactance changes from their original value to a range of values before a flaw is corrected. Net impedance may change if switching approaches solves the problem. Thus, SC current readings must be taken frequently when errors occur.^[22-24]

D. RCA(RCA)

Also consider the following criteria for system devices: The feeder's OC relay CC must be below overload and short circuit damage curves on the TCC scale. The feeder's over current relay coordination curve should be greater than its ampacity curve. The transformer's synchronization curve should be lower than its damage to structure and thermal damage curves. Ensure OC relay synchronization curves for XMERS exceed transformer ampacity curves and synchronize inrush stages. The generator's over current relay synchronization curve should be higher than its maximum load ampere curve and lower than the decrement and overload curves.

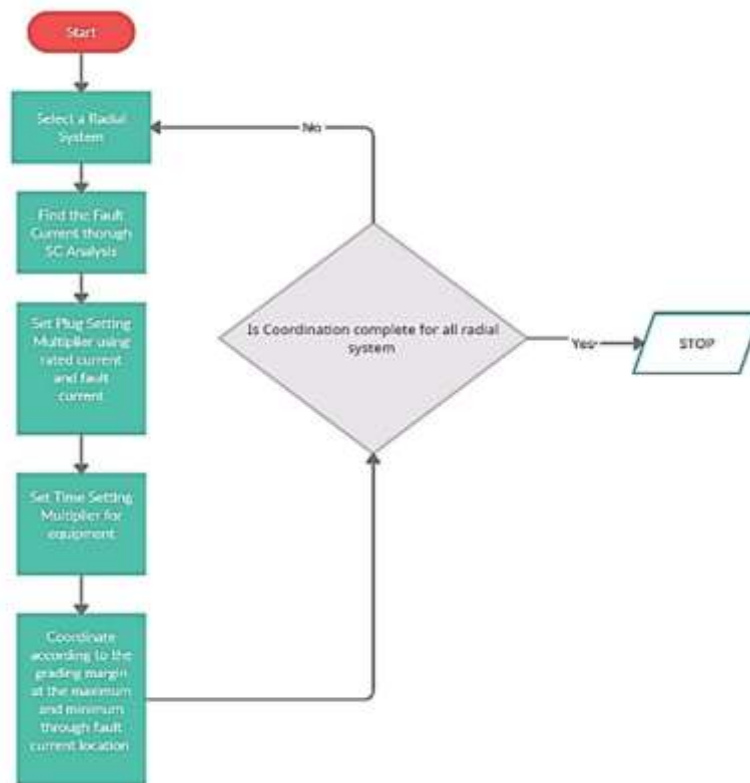


Fig 2: RCA Flow Chart

E. Reliability Assessment

By integrating these three basic indicators, namely the consumers connected at every loading point in a network and the customer disruption expense, it is possible to derive two extended sets of indices that encompass the size or significance of system failure. [30-32] There exists a collection of machine reliability indices.

$$SAIFI = \frac{\text{Total number of customer interruptions}}{\text{Total number of customers served}}$$

$$SAIDI = \frac{\text{Sum of all customer interruption durations}}{\text{Total number of customers served}}$$

$$CAIDI = \frac{SAIDI}{SAIFI} = \frac{\text{Sum of all customer interruption durations}}{\text{Total number of customer interruptions}}$$

$$ASAI = \frac{SAIFI}{SAIFI} = \frac{\text{Customer hours service availability}}{\text{Customer hours service demanded}}$$

$$ASUI = 1 - ASAI$$

These particular criteria are employed to assess the overall efficiency of the distribution system. The reliability cost/worth indices are an alternative set of measures. Expected Energy Not Supply (EENS),

$$EENS_i = P_i U_i$$

Expected Cost of Interruptions (ECOST),

$$ECOST_i = P_i \sum_j \epsilon_{Ne} f(r_i, j) \lambda e_j$$

$$IEAR = ECOST / EENS$$

Either of these indices assess the dependability of a functioning electricity supply and protection system, offering valuable strategic information for improving both existing and future distribution systems. Furthermore, the reliability indexes

EENS or ECOST can be analyzed by considering the element inputs and their respective rankings, which can provide insights into the index's susceptibility to component breakdown rates. It is possible to rate either just one load area or an entire structure with loads at various locations.

IV. RESULTS AND DISCUSSION

The LFA for the complete system has been shown below in the Fig 2 and Fig 3 describes the power flow at bus 7. From the FIG 4 its can clearly seen that total generation by each generations is 21.368 MVA, 28.451 MVA and 6.985 MW respectively, and total demand in the system is 41.134 MVA.

The SCA was performed on the system wherein the fault was generated at the various buses. Fig 4 shows the fault currents at bus 7 for LLL faults, LG faults, LL faults, and LLG faults. The LL fault current values are used then to set the CT ratio and pick up current for the analysis purpose.

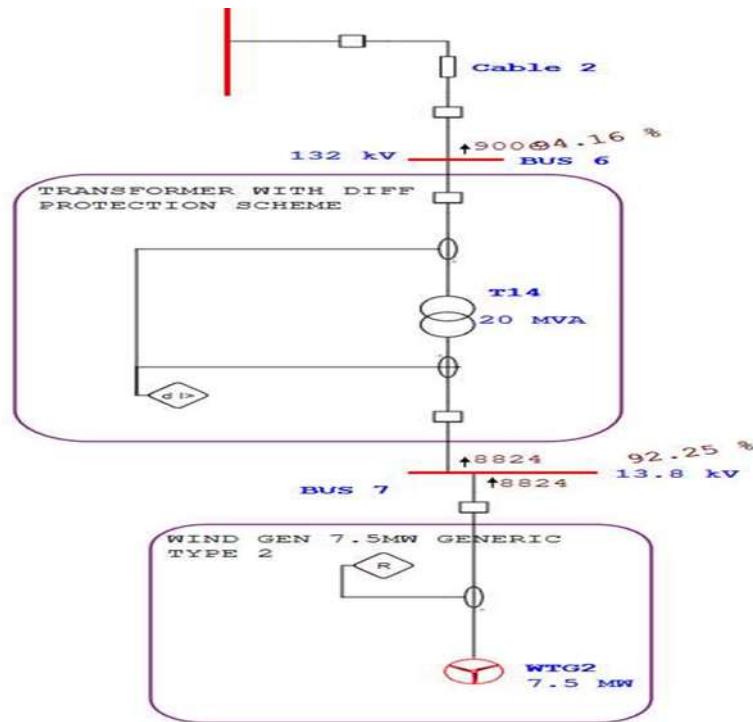


Fig. 3: LFA At bus 7

RA was performed on the entire system with Average Failure Rate and Average Outage Duration. AFR, PFR and MRR for the CB are 0.0156, 0.1298, and 194.125, respectively. The Mean Time to Failure (MTTF) is determined automatically using λ_A and λ_P and is 27.5 years, while the default MTTR is 5.6 hrs. Relay coordination using Star View was successful. System relay sequences are coordinated by the sequence analyzer. Fig 6 shows relay coordination when bus 7 faulted. First, relay 12 near bus 7 functioned at fault current of 2.458 kA at 11ms. A 70-ms C.B. 21 trip with OC50 forwarded. Fig 8 shows CB operating when a transformer fault was detected and relay coordination was established. Isolating the problematic system from the healthy system showed that the CB tripped in the correct sequence. The TCC for the WTG System shows that Relay no twelve is regarded with the Very Inverse Time Characteristic with OC67 as Directional Overcurrent Relay safety for the transformer. The location used ALSTOM P343 manufacturer MiCOM. The Fig shows Relay 12 parameters like PSM, TDS, and others. The ground fault TCC curve is shown in Fig 11, whereas the phase fault curve is shown in Fig 9.

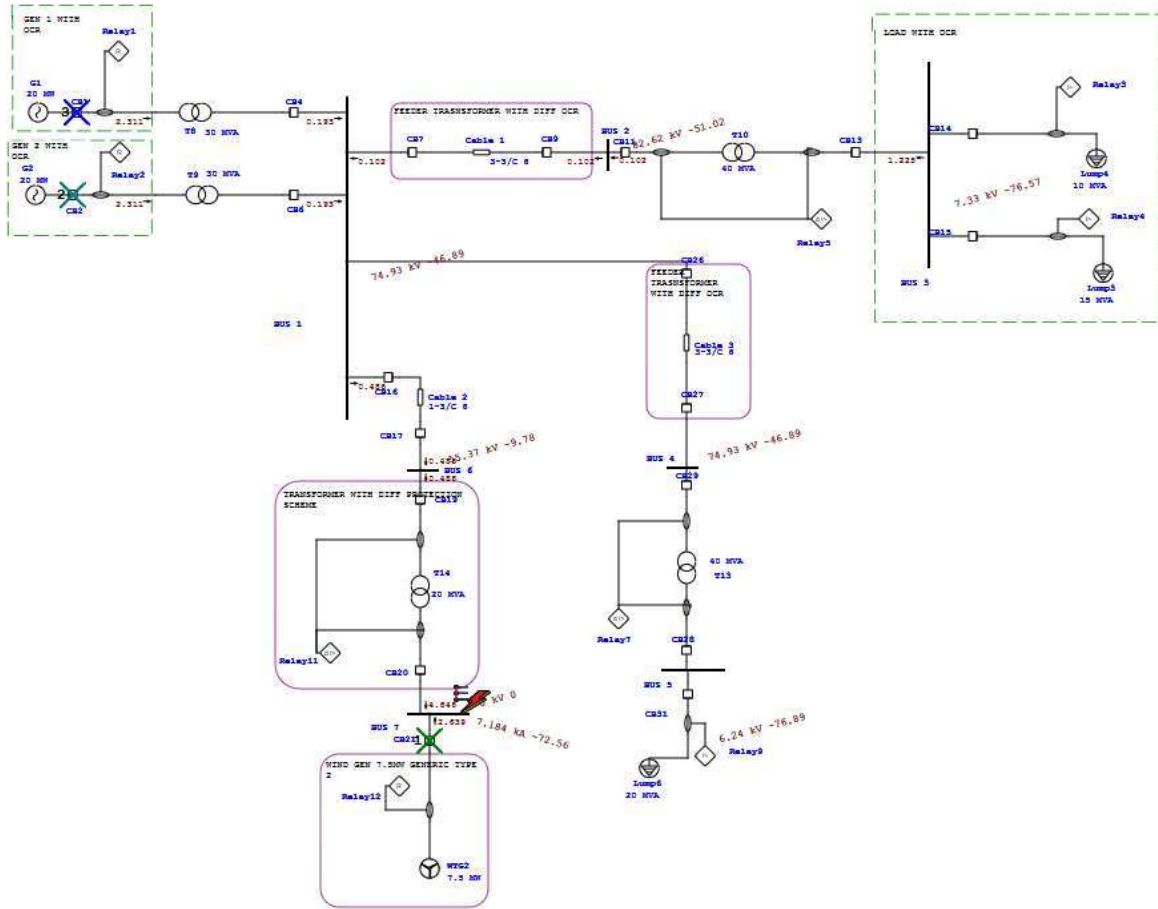


Fig 4: RCA at 7 bus

Sequence-of-Operation Events - Output Report: Untitled

3-Phase (Symmetrical) fault on bus: BUS 7

Data Rev.: Base Config: Normal Date: 26-05-2021

Time (ms)	ID	If (kA)	T1 (ms)	T2 (ms)	Condition
10.0	Relay12	2.639	10.0		Phase - OC1 - 50 - Forward
70.0	CB21		60.0		Tripped by Relay12 Phase - OC1 - 50 - Forward
149	Relay2	2.311	149		Phase - OC1 - 51
169	CB2		20.0		Tripped by Relay2 Phase - OC1 - 51
700	Relay1	2.311	700		Phase - OC1 - 51
760	CB1		60.0		Tripped by Relay1 Phase - OC1 - 51
3197	Relay12	2.639	3197		Phase - OC1 - 51 - Forward
3257	CB21		60.0		Tripped by Relay12 Phase - OC1 - 51 - Forward

Fig 5: Sequence of Operation of Events when fault at bus 7

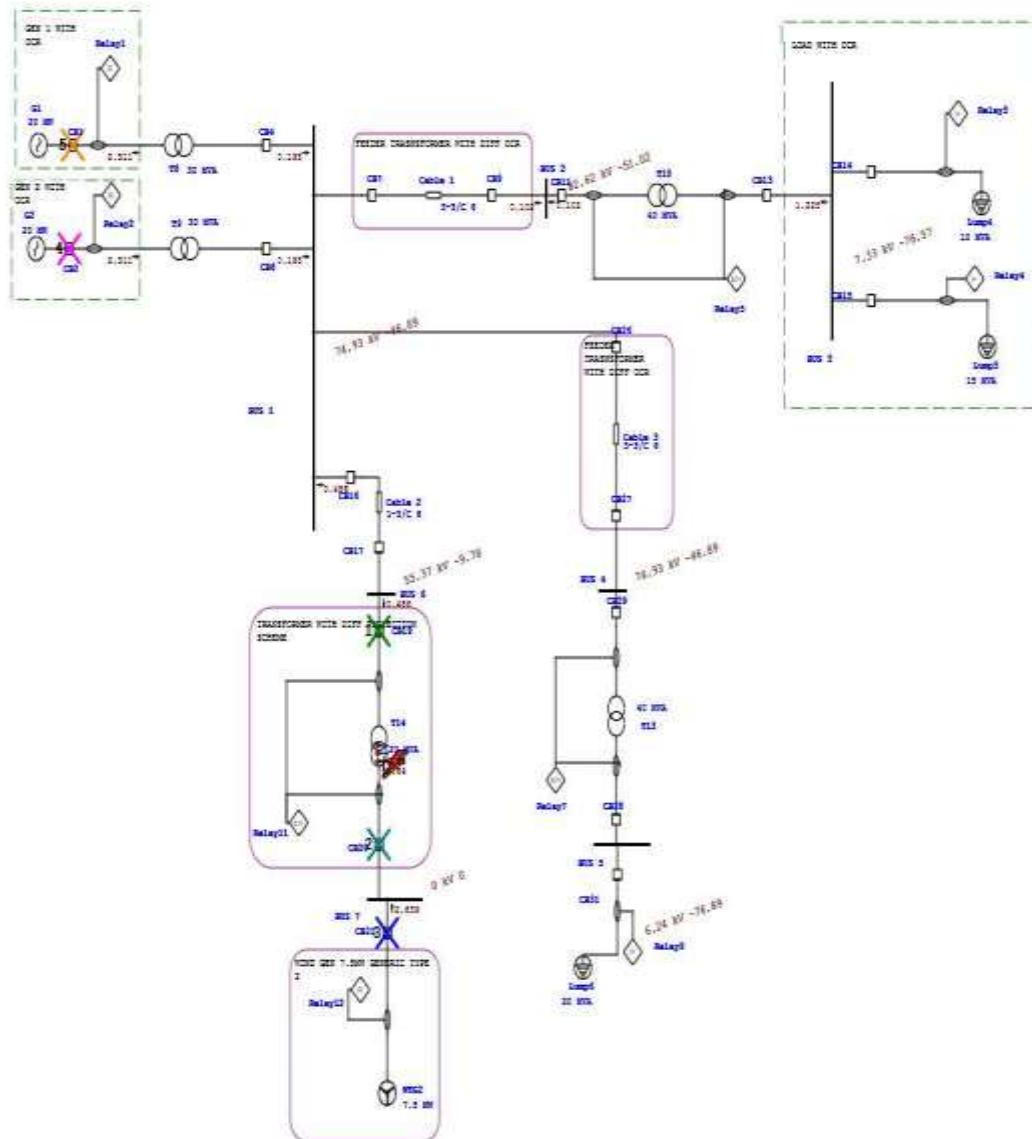
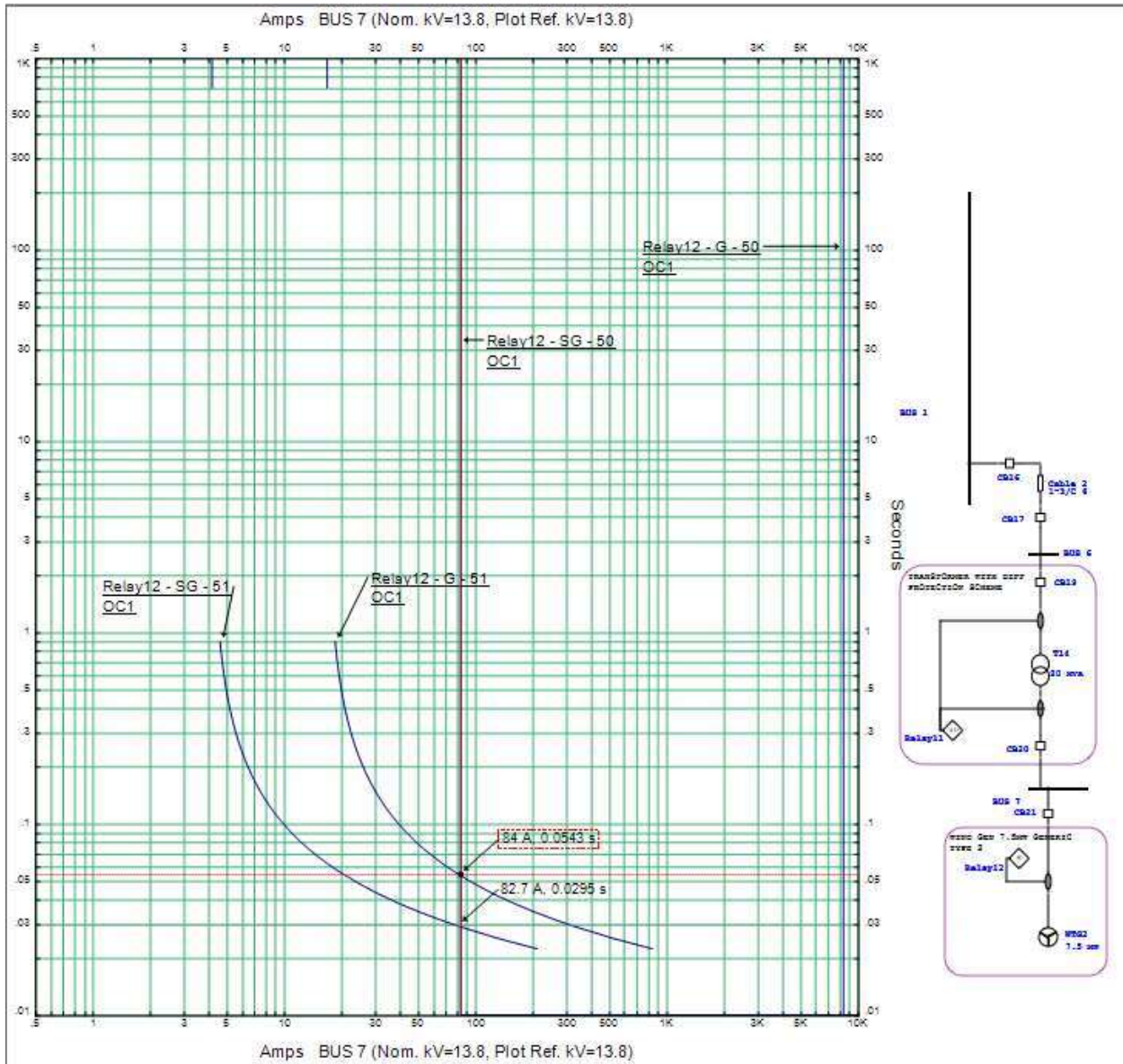


Fig 6: RCA for internal Fault



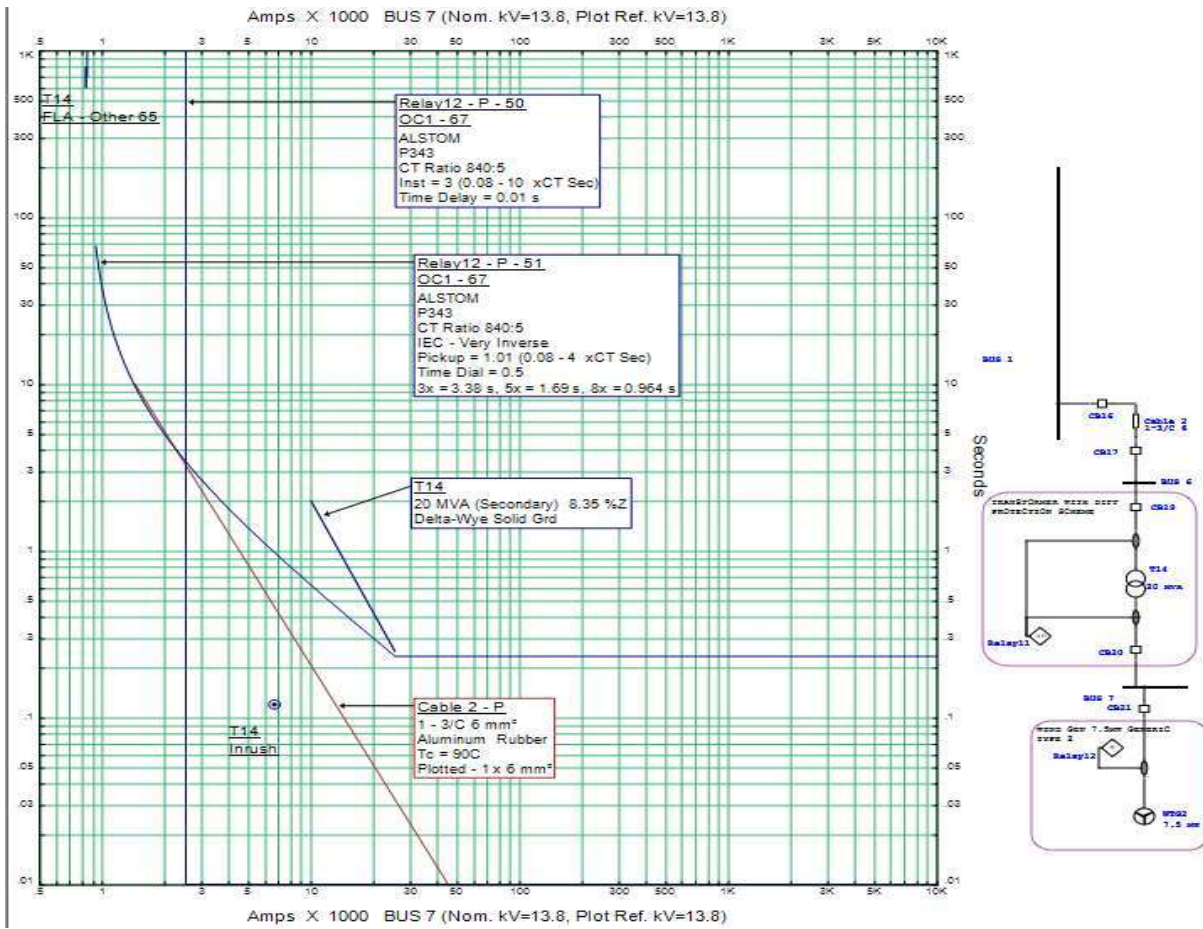


Fig 8: TCC for WTGS

V. CONCLUSION

As shown in the previous sections, the system's LFA, SCA, RA and RCA results show that relay coordination requires more than just setting relay settings. LFA is utilized in the RCS to determine and modify relay, circuits breakers, and current transformer configurations by estimating the average power flow, crucial and margin status of components, as well as the SCA values. A specialized approach coordinates relays and CBs in WTG systems. Coordination issues plague WTG integration. Maxing out the relay's pickup, clock dial, trip device, and low voltage circuit breaker promotes synchronization. Dependability tests measure network security without upsetting clients. ETAP simulates. Multiple safety procedures are activated after a 3-phase or single L-G failure. Using a consistent way to evaluate coordination and dependability for a large integrated system is tough. ETAP software improves speed and accuracy by reducing manpower and protective device failure. System reliability enhanced. Improving vast, linked power network safety yields greater results.

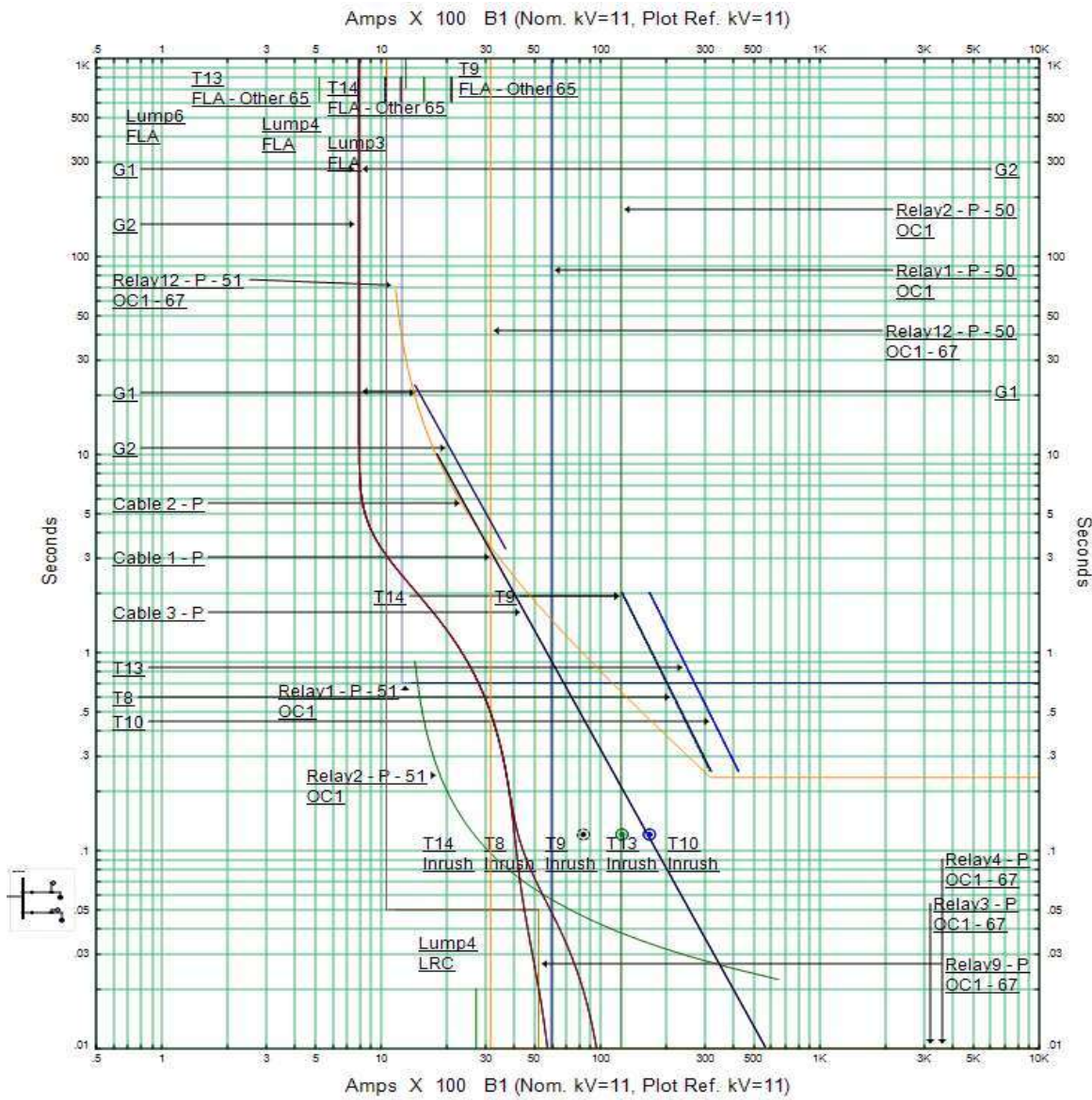


Fig 9: Overall TCC Curves

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