



Design and Manufacturing of Emergency Exit Device

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ABSTRACT

Emergency exit devices are crucial components of building safety systems, providing a means for rapid egress during emergencies such as fires or other disasters. This paper presents the design and manufacturing process of an innovative emergency exit device aimed at enhancing user safety and ease of use. The design phase begins with a comprehensive analysis of user needs, building codes, and safety regulations. Utilizing advanced CAD software, various design iterations are explored to optimize functionality, durability, and aesthetics. The device incorporates features such as intuitive operation, clear signage, and robust construction to ensure reliability in emergency situations. The manufacturing process employs state-of-the-art techniques such as 3D printing, CNC machining, and injection molding to produce high-quality components with precision and efficiency. Materials selection focuses on durability, fire resistance, and environmental sustainability, aligning with modern safety standards and regulations. Quality control measures are implemented throughout the manufacturing process to guarantee adherence to specifications and standards. Prototypes undergo rigorous testing procedures, including functionality tests, load tests, and fire resistance tests, to validate performance and reliability.

Keywords : Design and manufacturing of emergency exit from refuge area of building (Sky Saver)

I. INTRODUCTION

Ensuring the safety of occupants within buildings during emergencies is paramount in modern architecture and construction. Emergency exit devices serve as vital components of building safety systems, facilitating rapid egress during critical situations such as fires, natural disasters, or other emergencies. This paper delves into the meticulous process of designing and manufacturing an innovative emergency exit device, with a primary focus on enhancing user safety and ease of use.

The design phase of the emergency exit device entails a comprehensive analysis that considers various factors, including user requirements, building codes, and safety regulations. Leveraging advanced Computer-Aided Design (CAD) software, designers explore multiple iterations to optimize functionality, durability, and aesthetic appeal. Central to the design is the integration of intuitive operation, clear signage, and robust construction to ensure the device's reliability and effectiveness during emergencies.

Subsequently, the manufacturing process employs cutting-edge techniques such as 3D printing, Computer Numerical Control (CNC) machining, and injection molding to fabricate high-quality components with precision and efficiency. Material selection plays a pivotal role, emphasizing attributes such as durability, fire resistance, and environmental sustainability, aligning with contemporary safety standards and regulations.

Quality control measures are rigorously implemented throughout the manufacturing process to ensure adherence to specifications and standards. Prototypes undergo exhaustive testing procedures, including functionality tests, load tests, and fire resistance tests, to validate performance and reliability under simulated emergency conditions.

In summary, the design and manufacturing of this emergency exit device epitomize a holistic approach to safety engineering. By amalgamating innovative design concepts with advanced manufacturing techniques, the resulting product prioritizes user safety while adhering to stringent regulatory requirements. This endeavor underscores the commitment to safeguarding lives and property in the face of unforeseen emergencies within built environments.

Methodology

- Introduction of concept
- Designing of simple mechanism for reuse it by any person
- Select material rope, brake and all components
- Mathematical calculation of size for every component
- CAD design of each and every component

- Manufacture sky saver for the obtained parameters
- Testing of the sky saver by dead weight and generate result table and

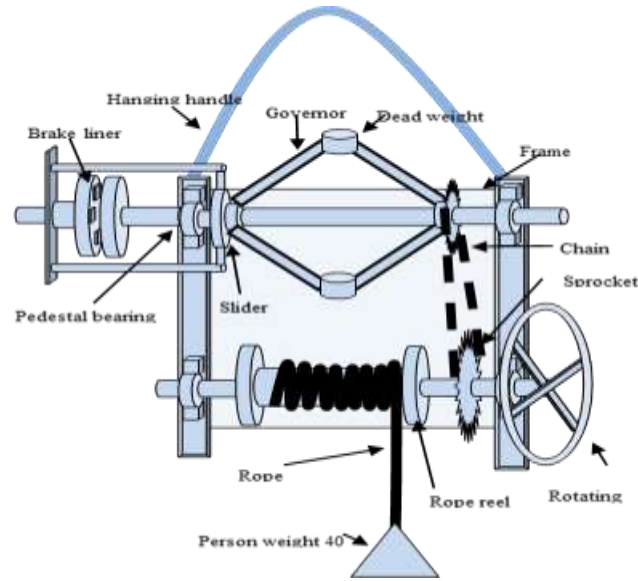


Fig. 1 - (a) 2d Working methodology

Calculation

Let us design the machine for caring 100 kg weight and downfall speed of 2 m/s

Rope selection

The relationship between mass and force (weight) can be expressed as: $m = f/g$

Where,

F = force, weight (N)

m = mass (kg)

g = acceleration of gravity (9.81 m/s²)

Maximum safe mass for a 3/8" nylon rope where safe load is 1.2 KN can be calculated as

$$m = (1.2 \times 1000 \text{ N}) / (9.81 \text{ m/s}^2)$$

$$= 122 \text{ kg}$$

So, the rope we chose is a nylon rope and it can carry maximum 122 kg > 100kg

The expression $\sqrt{M^2 + T^2}$ is known as *equivalent twisting moment* and is denoted by T_e . The equivalent twisting moment may be defined as that twisting moment, which when acting alone, produces the same shear stress (τ) as the actual twisting moment. By limiting the maximum shear stress (τ_{\max}) equal to the allowable shear stress (τ) for the material, the equation (i) may be written as

$$T_e = \sqrt{M^2 + T^2} = \frac{\pi}{16} \times \tau \times d^3 \quad \dots (ii)$$

1.Reel shaft des

The total weight on shaft coming is: -

$$W=100 \text{ kg}= 981 \text{ N}$$

$$M= w \times L/4 = 981 \times 300/4 = 73575 \text{ N-mm}$$

$$T = f \times r \text{ (reel radius)} = 981 \times 30 = 29430 \text{ N-mm}$$

$$T_e = \sqrt{M^2 + T^2} = \sqrt{73575^2 + 29430^2}$$

$$\text{Also, } T_e = \pi/16 \times 135 \times d^3$$

$$\text{So, } 79242.70 = \pi/16 \times 135 \times d^3$$

$$d = 14.40 \text{ mm}$$

$$\text{So, } d = 15 \text{ mm}$$

But we are using 20mm shaft so design is safe. $20\text{mm} > 15\text{mm}$.

2. Bearing selection

For 20mm Shaft diameter we take standard bearing no. P204

P204: -

P = Pedestal bearing.

2 = Spherical ball or deep groove ball bearing

$$= 04 = 5 * 4 = 20 \text{ mm.}$$

20mm = Bore diameter of bearing.

3. RPM of reel shaft

d = diameter of reel

$$V = 2 \text{ m/s}$$

$$\text{Linear velocity } V = \pi \times d \times N / 60$$

$$2 = 3.142 \times 0.06 \times N / 60$$

$$\text{So, } N = 636 \text{ rpm}$$

4. RPM of governor shaft

$$\text{Pulley Ratio} = 250/100 = 2.5$$

$$636 \times 2.5 = 1590 \text{ RPM}$$

5. Number of V-Belts

We know that the power transmitted per belt,

$$P = (T_1 - T_2) \times V$$

As we know maximum torque on shaft = $T_{\text{max}} = T = 29430 \text{ N-mm}$

Where,

T_1 = Tension in tight side

T_2 = Tension in slack side

O1O2 = centre distance between two shafts

$$\sin \alpha = \frac{R_1 - R_2}{O_1O_2}$$

$$\sin \alpha = \frac{125 - 50}{310}$$

$$\sin \alpha = 0.2419$$

$$\alpha = 14$$

TO FIND θ

$$\theta = (180 - 2\alpha) \times 3.14/180$$

$$\theta = (180 - 2 \times 14) \times 3.14/180$$

$$\theta = 2.652 \text{ rad}$$

we know that,

$$T_1/T_2 = e^{\mu\theta \operatorname{Cosec} \beta}$$

$$T_1/T_2 = e^{0.25 \times 2.652 \operatorname{cosec} 20}$$

$$T_1 = 6.95T_2$$

We have,

$$T = (T_1 - T_2) \times R$$

$$29430 = (6.95T_2 - T_2) \times 125$$

$$T_2 = 39.57 \text{ N}$$

$$T_1 = 6.95 \times 39.57$$

$$T_1 = 275 \text{ N}$$

So, tension in tight side = $T_1 = 275 \text{ N}$

$$V = \pi DN/60$$

$$= 3.142 \times 0.125 \times 636/60$$

$$V = 4.16 \text{ m/sec.}$$

$$P = (275 - 39.57) \times 4.16$$

$$P = 979.39 \text{ W (N-m/s)}$$

Also, $P = 2\pi NT/60$

$$P = 1960.08$$

Number of V-Belts: -

$$N = \text{Total Power transmitted} / \text{Power transmitted per belt}$$

$$= 979.39/1960.08 = 0.499$$

$$= \text{Say 1 belt}$$

So, 1 belt is sufficient for transmission of power

Calculation on length of belt

We know that radius of pulley on shaft,

$$r_1 = d_1/2 = 250/2 = 125 \text{ mm}$$

Radius of pulley on motor shaft,

$$r_2 = d_2/2 = 50/2 = 50 \text{ mm}$$

Centre distance between two pulley = 305 mm

We know length of belt,

$$\begin{aligned} L &= \Pi (r_2 + r_1) + 2 \times X + (r_2 - r_1)^2 / X \\ &= \Pi (125 + 50) + (2 \times 310) + (125 - 50)^2 / 310 \end{aligned}$$

$$L = 1143 \text{ mm} = 45 \text{ inches}$$

(1)

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