



# Design of a Compact Dual Notched Semi Circular Shaped UWB Antenna

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## ABSTRACT

This paper presents the design of a miniaturized Ultra-Wideband (UWB) antenna with dual band notched and low specific absorption rate (SAR) for body-centric wireless communication applications. The proposed antenna operates from 3.4 GHz to 14.2GHz with two notched frequencies at 5.4-5.6 GHz (Wi-Fi/ISM) and 6.5 GHz - 8.2 GHz (Wimax). The antenna's dimensions were optimized using genetic algorithm embedded in the HFSS and CST software used to achieve a compact size of 26 mm × 27 mm in semi-circular shape with radius 12mm. The SAR value was reduced by using a defected ground structure (DGS) and rectangular slots. Simulation results show that the antenna achieves a return loss of -10 dB, a minimum gain of 5 dBi and maximum gain of 7dBi at 8GHz frequency which is an indication that the proposed antenna is suitable for UWB applications.

Key words: UWB, SAR, Substrate, notched bands, body centric

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## 1. INTRODUCTION

Antenna in wireless communication are of different types depending on the area of applications including Omni-directional antenna which radiates equally in all directions e.g. dipole and monopole, Directional antenna which focuses radiation in a specific direction e.g. parabolic and horn antenna, Semi directional antenna which combines Omni directional and Directional characteristics e.g. patch antenna and Array antenna which are multiple antennas combined for improved gain and directivity. Also in place nowadays are smart antennas which adaptively adjust beam pattern for optimal performance. But because of ease of construction low cost and other advantages patch antenna are commonly employed in wearable applications.

Ultra Wide Band (UWB) antenna have the advantages of Wide bandwidth as they operate over a wide frequency range (3.1-10.6 GHz), enabling high-data-rate transmission, they also have Low power consumption UWB antennas require lower transmission power, reducing interference and SAR (Specific Absorption Rate) values, another advantage is their comparative high gain and efficiency due to their wide bandwidth.

In their own words, Kraus, J. D., & Marhefka, R. J. (2002) defined an antenna as device that radiates or receives electromagnetic energy, and is used for communication, navigation, or other purposes." IEEE Standard 145-2013: "An antenna is a device that converts electrical energy into electromagnetic waves and vice versa, enabling communication between devices." Furthermore International Telecommunication Union (ITU) - Recommendation ITU-R V.117-4: "An antenna is a device, or system of devices, used to transmit or receive electromagnetic waves, and is an essential component of a telecommunication system."

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## 2. LITERATURE REVIEW

### 2.1 ANTENNA DESIGN FOR UWB APPLICATIONS

#### ULTRA WIDE BAND (UWB) ANTENNA

An ultra-wideband (UWB) antenna is a device that receives signals in the frequency range between 3.1 GHz to 10.7 GHz. With the rapid development of communication technology, ultra-wideband (UWB) communication system has gained the attention and focus of researchers. UWB requires that the relative bandwidth ratio is higher than 20%, or the absolute bandwidth is greater than 0.5GHz (Chen, Z. N., et al 2004). According to Federal Communications Commission (FCC) regulations, UWB communication systems can use the frequency band from 3.1GHz to 10.6GHz. The available frequency band usually includes several civil narrowband communication bands, such as C-band satellite uplink/downlink band (5.925–6.425/3.7–4.2GHz), wireless local area network (WLAN) band (5.15–5.35GHz, 5.725–5.825GHz), and X-band satellite uplink/downlink band (7.9–8.4/7.25–7.75GHz). As the narrowband communication system occupies part of the UWB, the mutual interference between them is inevitable, so band notch UWB antenna has great research value FCC. (2002).

There are different types of UWB antennas (Guha, D., & Antar, Y. M. M.2011)

### **REVIEW OF PAST WORKS**

Manjunathan et al (2024) carried out performance analysis of microstrip patch antenna for wireless communication. Their research showed that microstrip patch antenna had been focus of researchers in the field of wireless communication with over 1500 research articles, and textbooks on the subject matter due largely to the comparative advantages it has over other types of antenna like compactness, large bandwidth and high gain advantages. Their work showed that bandwidth of a patch antenna can be improved by thickening the substrate level, though they also found out that this may have the disadvantage of minimizing the efficiency of the antenna due to less power radiation occasioned by the significant amount of input power waster in the resistor. These identified flaws were compensated for using electromagnetic band gap (EBG) structure with their unique characteristics which increases efficiency by as high as 48.8% in bandwidth.

Furthermore, Anees Abbas et al (2020) realized a compact ultra-wideband (UWB) antenna of optimized dimension of size of the compact antenna is  $16 \times 25 \times 1.52$  mm<sup>3</sup> by using rectangular notch wireless area network (WLAN) band with controllable notched bandwidth and center frequency. They achieved UWB characteristics of the antenna by truncating the lower ends of the rectangular microstrip patch; they also used electromagnetic bandgap (EBG) structures to obtained notch characteristics of the antenna. EBG is made up of two rectangular metallic conductors mounted on the back of the radiator, and connected to the patch by shorting pins. They tuned the individual resonant frequencies of the EBGs and merged them rectangular notch to realize WLAN band with high selectivity. Their results show that the bandwidth and frequency of the rectangular notch band Their simulated and measured results show that the antenna has an operational bandwidth from 3.1–12.5 GHz for  $|S_{11}| < -10$  with a rectangular notch band from 5–6 GHz, thus rejecting WLAN band signals. Their results also showed that the antenna stable gain and radiation patterns.

Subhash et al (2024) used two bevels of a semi-circle engraved with stepped cut monopole antenna to develop a reconfigurable multiband notched semi-circle engraved UWB antenna for wireless communication application. They used L-shaped and Ladder shaped stubs of quarter wavelength on the patch to achieve notching characteristics in the 5G band of 3.40 – 3.70 GHz (n78) and 4.84 – 5.70 (n46). By also incorporating a half wavelength C-shaped slot and I-shaped stub on the patch, they were able to achieve another notch band at 3.88 – 4.32 (n77, C band) and 7.10 – 7.61 GHz (X band, satellite downlink). Subhash (2024) also used eight PIN diodes to regulate the multi operations modes which allows it to switch into single/double/triple/quadruple m band notch characteristics. The overall dimension of their work is 0.2 x 0.37 mm<sup>2</sup> using Rogers RT/duroid 5880 substrate. Their simulated and measured, and calculated equivalent circuit showed significance agreement in terms of high gain, stable radiation pattern all through the UWB band.

In addition, Azza Elnaggar (2024) reported the development of a textile two port multiple input multiple output MIMO half circle UWB antenna with corrugated borders for biomedical diagnostics applications. In their work they used orthogonal polarization technique to reduce the mutual coupling effect, enhance signal quality and make imaging more accurate. They injected a low pass filter for out of band rejection using a 50 ohms coplanar waveguide as elements. The antenna was developed on textile materials using conducting fabrics to achieve flexibility for the antenna. The dielectric material used was cotton of tangent value 0.0025. The optimized dimension was 40 x 40 x 0.3 and their results showed a wide bandwidth of between 2.5 – 12 GHz coupled with omnidirectional radiation pattern, maximum gain of 6dBi and 96% efficiency.

Sesha Vidhya (2023) analyzed the performance of a triple band miniaturized hexagonal UWB antenna for wireless body worn applications to mitigate the significant challenges human body causes for both wearables and implantables antenna devices. The antenna was fabricated using FR4 substrate with dimensions with dimensions 24 x 25 x 1.6 and they achieved a frequency bandwidth of 3 – 9 GHz with a reflective coefficient of -15dB and gain of 2.5dBi. They also found the antenna SAR to be 2 W/kg and without SRR were found to be 3.5 W/kg.

## **3.1 METHODOLOGY**

Standard equations for patch antenna (as shown in equations 1 to 7) were used to design the dimensions of the various parts of the antenna. The design was optimized using HFSS and CST studio software leading to a compact, miniaturized UWB antenna that is significantly safe in terms of radiation effect on human body. Theory of size optimization, rejection of interference bands using slot notching techniques to eliminate undesirable frequency bands and careful selection of substrate materials to improve the SAR the antenna were all applied in achieving the design objective of the proposed antenna.

### **3.2 ANTENNA CONFIGURATION**

The designed antenna consists of FR4 substrate with permittivity ( $\delta$ ) of 4.4 and thickness of 1.6mm as dielectric material, semi-circular patch with a H slot, defected ground structure (DGS), rectangle microstrip feed line, two notched frequencies achieved using a H-shaped slot for 5.15-5.825 GHz and a U-shaped slot for 7.725-8.275 GHz.

### **3.3 DUAL NOTCHED FREQUENCY UWB ANTENNA DESIGN**

To design the proposed antenna the following methods were undertaken step by step viz:

- i. determination of antenna size and shape by calculations using standard equations iii – vi,

- ii. optimization of the calculated sizes and shape using genetic algorithm embedded in HFSS and CST software through multiple iterations and simulations of different sizes and shapes of designed patch antenna and comparing results to achieve desired compactness,
- iii. achieve desired bandwidth of at least 10 GHz with desired gains at different frequencies and other performance evaluation metrics by using ground defected structure (GDS) technique,
- iv. notching of undesirable frequency bands of ISM of frequency and WIMAX of frequency bands using H and U slots in the patch and the feed line,
- v. careful selection of the optimal substrate of the dielectric material to achieve low SAR and compactness of the antenna by simulating the antenna and analyzing the results using different substrate materials.

### 3.4 ANTENNA DESIGN CALCULATIONS

The radiating patch, the feedline, and the ground of the antenna dimensions were calculated as shown in the equations iii - x

The effective radius of the patch is given by

$$a_e = a \left[ 1 + \left[ \frac{2h}{\pi\epsilon_r} \right] \ln \left[ \frac{\pi a}{2h} \right] + 1.7726^{1/2} \right] \quad (1)$$

### 3.5 RADIUS OF THE PATCH

FR4 (lossy) as the substrate has a permittivity  $\epsilon_r$  of 4.4, and height of dielectric optimized as 1.6mm. The dimension of the semi-circular patch is calculated using equations...

$$\lambda = \frac{c}{f_0 f_r} \text{ where } f_0 = \frac{3 \times 10^8}{2.4 \times 10^9} = 0.125 \text{ mm} \left[ \epsilon_{reff} \frac{\epsilon_{reff} + 0.3}{\epsilon_{reff} - 0.258} \frac{(\epsilon_{eff} + 3) \left( \frac{W}{h} + 0.264 \right)}{(\epsilon_{eff} - 0.258) \left( \frac{W}{h} + 0.8 \right)} \right] \quad (2)$$

The semi-circular patch antenna radius is determined from the expression

$$a = \frac{F}{\left[ 1 + \left[ \frac{2h}{\pi\epsilon_r} \right] \ln \left[ \frac{F}{2h} \right] + 1.7726 \right]^{1/2}} \quad (3)$$

$$W = \frac{c}{2f_r \sqrt{\frac{\epsilon_r + 1}{2}}} = \quad (4)$$

The length of the patch of the antenna is given as equation

$$L = L_{eff} - 2\Delta L \quad (5)$$

where

$$L_{eff} = \frac{c}{2f_r \sqrt{\epsilon_{reff}}} \quad (6)$$

Where effective dielectric constant  $\epsilon_{reff}$

$$\epsilon_{reff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[ 1 + 12 \frac{h}{W} \right]^{-1/2}$$

$$\text{The length extension } \Delta L = 0.412h \times \left[ \epsilon_{reff} \frac{\epsilon_{reff} + 0.3}{\epsilon_{reff} - 0.258} \frac{(\epsilon_{eff} + 3) \left( \frac{W}{h} + 0.264 \right)}{(\epsilon_{eff} - 0.258) \left( \frac{W}{h} + 0.8 \right)} \right]$$

We can also calculate the effective dielectric constant from the equation

$$\epsilon_{reff} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[ 1 + 12 \frac{h}{W} \right]^{-1/2}$$

Calculation of the length of extension is

$$\Delta L = 0.412h \times \left[ \epsilon_{reff} \frac{\epsilon_{reff} + 0.3}{\epsilon_{reff} - 0.258} \frac{(\epsilon_{eff} + 3) \left( \frac{W}{h} + 0.264 \right)}{(\epsilon_{eff} - 0.258) \left( \frac{W}{h} + 0.8 \right)} \right] \quad (7)$$

### 3.6 ANTENNA MODELLING SOFTWARE

EM simulation tools are used to predict antenna performance in a specific environment. There are a number of software that are available for modeling of antenna including CST-MS, HFSS and others. These software are based on different algorithms including Finite Distance Time Domain (FDTD) which algorithm is built on solving differential equations, Finite Integration technique (FIT) which is integral equation based, Methods of Moments (MoM) which is also based on solving integral equation and Finite Element Method (FEM) which algorithm is based on differential equation. In this work HFSS and CST software were used for size and shape optimization simulations and performance metrics analysis

Using the calculated values the antenna was designed using different shapes with the sizes and the optimized size and shape after analyzing all the simulations results are summarized in table and shown in table 1

Parameter	Value (mm)
Radius of patch (R)	13
X position (Xp), Y position (Yp) of patch	-12 , 0
Length of substrate (L)	27
Width of substrate (W)	26
Partial ground plane (L <sub>p</sub> )	11.5
Width feed line (W <sub>f</sub> )	3
Length feed line (L <sub>f</sub> )	13
Length of slot (L <sub>s</sub> )	3
Width of slot (W <sub>s</sub> )	4
Width of U slot (W <sub>Us</sub> )	5
Length U slot (L <sub>Us</sub> )	4.45
Length of H slot (L <sub>Hs</sub> )	6.4
Width of H slot (L <sub>Hs</sub> )	7.77

The designed antenna using HFSS software with these optimized dimensions given in the table 1 is as shown in figure 1



Figure 1: Antenna patch and feedline



Figure 2: Antenna ground

The antenna shown in figures 1 and 2 were subjected to parameter analysis to determine the performance and it was discovered that the S<sub>1,1</sub> parameters showed that the bandwidth of operation of this antenna was low as it was between 3GHz and 9 GHz which translates to just 6GHz of bandwidth. In order to improve this, further modification of the antenna was necessary and the method employed was to create a defected ground that will increase the bandwidth. This was achieved by cutting the ground into half and using ground defected structure at the centre of the ground of the antenna with dimension 3mm x 4mm as shown in figures 3 and 4 respectively.



Figure 3: Antenna ground halved

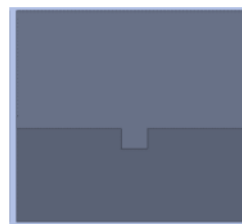


Figure 4: Antenna ground with DGS slot

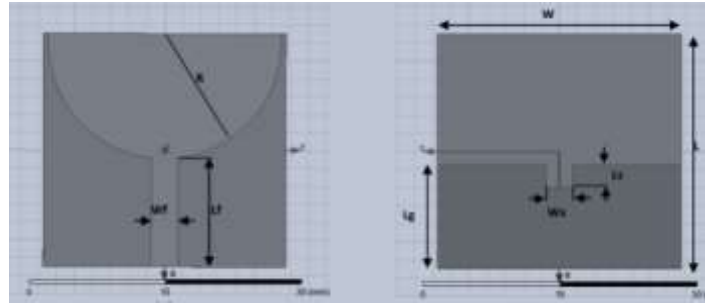


Figure 5: Antenna geometry showing radiator and feedline

Figure 6: Antenna ground geometry with DGS slot

Geometry of the antenna (figures 5 and 6) before the notching slots H and U were introduced in the patch and the feed line respectively.

To create the rejection of unwanted bands of frequencies which were ISM and WIMAX bands, chosen purposely to avoid interference of the antenna when being used for on body applications in different environments, two slots H with dimensions were cut in the radiating patch and U with dimensions were cut in the feed line as shown in figure 5, 6 and 7

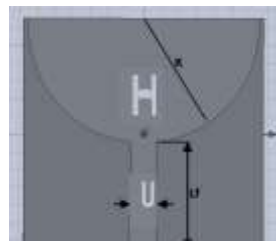


Figure 7: Geometry of with notching slots H and U were introduced in the patch and the feed line

#### 4.1 RESULTS AND DISCUSSION

The following graphs show the performance of the antenna at the three different stages of the design viz;

Stage i: Antenna design with the optimized dimensions without slots

Stage ii: Antenna halved with DGS slot in the ground

Stage iii: Antenna with H and U slots for dual frequency notched

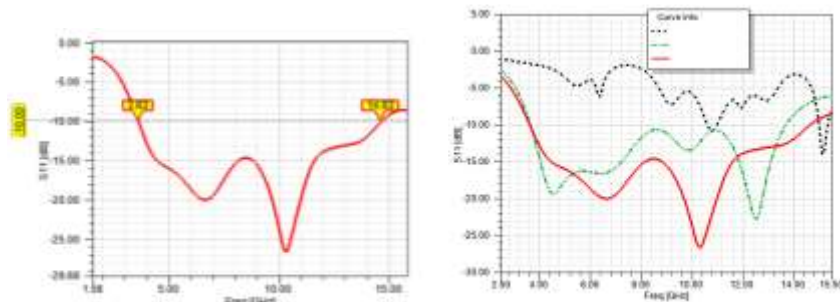


Figure 8 and 9: S11 plots of the three stages of the design of the antenna

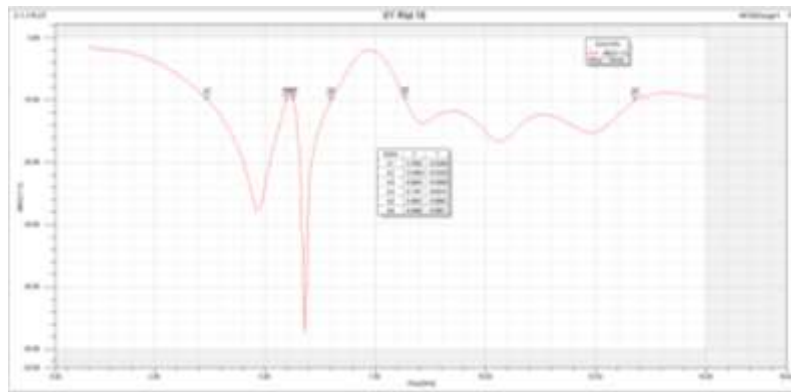


Figure 10: Reflection coefficient or return loss of the antenna plot

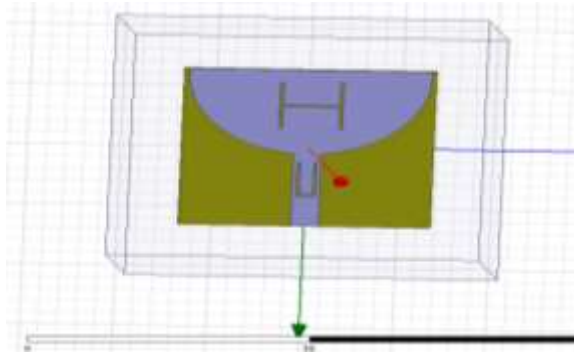


Figure 11: Front view of the design in HFSS

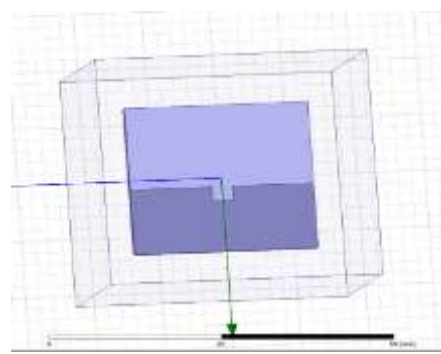


Figure 12: Back view of the design in HFSS

Figure 10 shows the S1,1 plot of the antenna, this reflection coefficient also called return loss is a critical parameter in evaluating the performance of a UWB antenna as it represents the ratio of the reflected wave to the incident wave at the antenna's input port. It also indicates the impedance matching between the patch and the feedline. In other words the S11 determines the bandwidth of the antenna, the antenna efficiency and impedance matching. The result from simulation showed that between the frequency bands 3.2GHz to 13.7 GHz there was a return loss of -10dB or less which indicates that the designed antenna achieved a 10.5GHz bandwidth which makes the antenna usable in ultra wide band (UWB) range. The plot also showed that the frequency between 3GHz -5.1GHz which is WIMAX band and ISM band were above -10dB were notched.

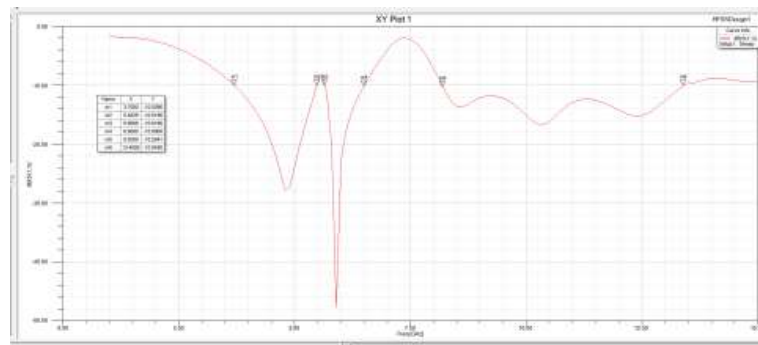


Figure 13: Reflection coefficient (S1,1) of the antenna showing double notches

Figures 14 to 16 showed the current distributions of the antenna in different frequency range between the operating bandwidth. The distributions showed that at the two notched frequency the concentration was strongest in figures which shows the bands were notched.

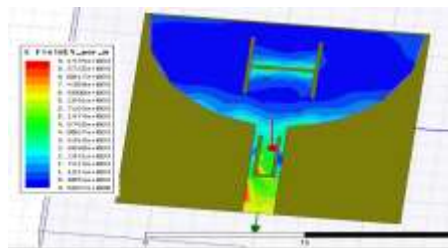


Figure 14: Surface current distribution

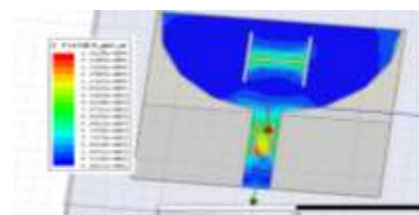


Figure 15: Surface current distribution Figure 16: Surface current distribution

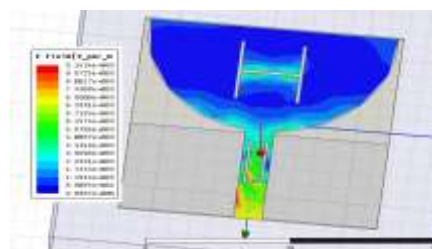


Figure 16 shows the radiation pattern of the antenna.

The plot showed that the antenna demonstrates a directional radiation pattern which is highly desirable for antenna used in body centric applications. Directional antenna will concentrate the radiation in a determined direction and this quality is explored in UWB to reduce the harmful effects of the EM radiation on human body by directing the radiation to a particular area without affecting other areas.

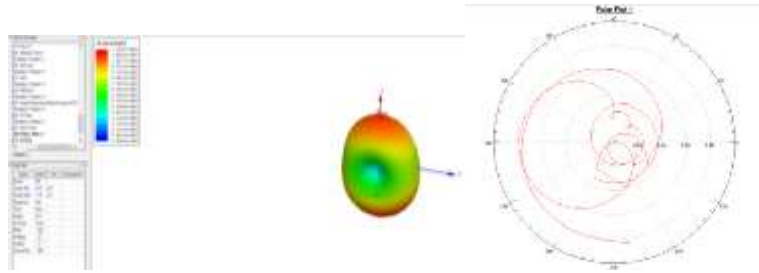


Figure 17: Radiation pattern of the antenna

The radiation pattern gain of the antenna was plotted at different frequencies and superimposed on one another to show the radiation patten in 2D as shown in figure 19 which also corroborates the 3D and Smiths chart plots results earlier shown in figure 17 and 18.

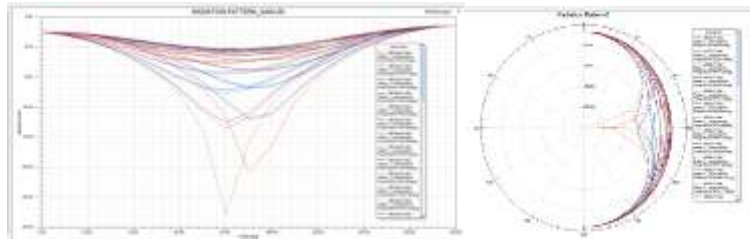


Figure 18: Radiation pattern of the antenna

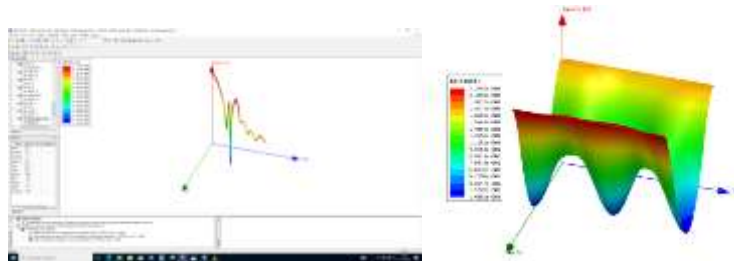


Figure 19: Radiation pattern of the antenna

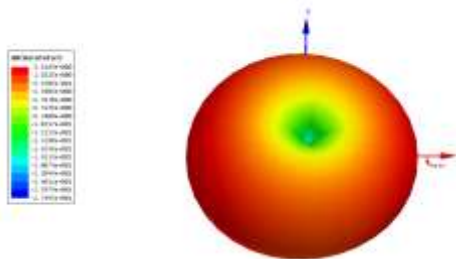


Figure 20: Radiation pattern of the antenna

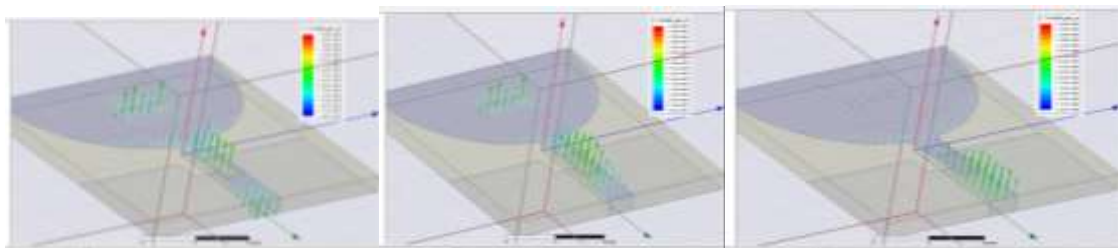


Figure 21: Field distribution plots of the antenna

The gain of the antenna was very high at frequencies with values ranging from as shown in stacked plots figures 22 and 23. The gain was tabulated for different frequencies in table 1

Theta (Deg)	Phi (Deg)	Gain (dBi)	Gain (dBi)	Gain (dBi)	Gain (dBi)	Gain (dBi)	Gain (dBi)	Gain (dBi)	Gain (dBi)
1	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
2	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
3	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
4	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
5	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
6	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
7	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
8	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
9	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
10	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
11	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
12	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
13	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
14	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
15	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
16	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
17	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
18	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
19	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712
20	0.00000	2.88745	2.88744	2.88739	2.88731	2.88726	2.88721	2.88717	2.88712

Table 1

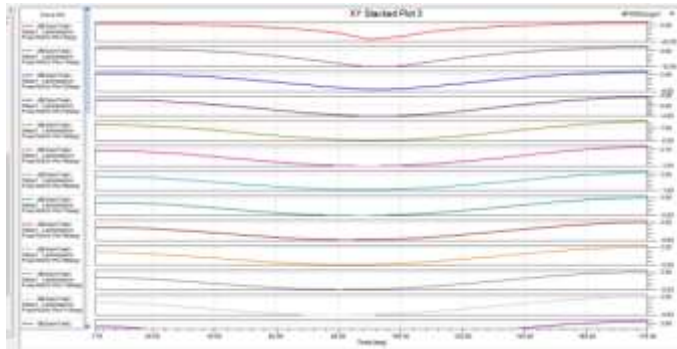
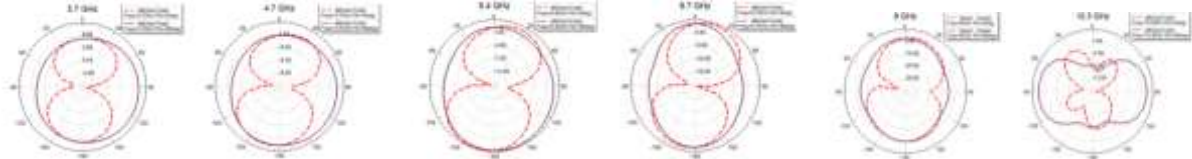


Figure 11: Stacked plot of radiation pattern of the antenna

Table 2: Data table of the Antenna gain for different frequencies



**5. CONCLUSION**

This paper presented the design of a dual notched frequency low SAR ultra wide band antenna for body centric application with an optimized overall dimension of 26 x 27 mm using FRA substrate. The dual band notched were achieved by cutting H and U slots in the radiator and feedline respectively and using a rectangular ground defected structure (DGS) at the ground plane. The bandwidth of operation the design achieved operated between the frequency range of 3.1 GHz to 13.8 GHz and with a maximum gain of 7 dBi at 8GHz. The proposed antenna exhibited a directional radiation pattern which was consistent in all the frequencies at various orientations of theta and phi angles. The simulation and experimental results showed that there was no significant variation between the simulated results and the experimental set up results indicating the developed antenna was very suitable for body centric purposes as it was compact, operated within a bandwidth of 10.5 GHz and low SAR of 1.6/10kg/w.

**RECOMMENDATION**

It is recommended that further works be carried out on UWB antenna design for body centric application by exploring the possibilities of integrating quantum optimization algorithm into the design process. Human phantom models were used in the simulation of this research, it is recommended that further works be done using actual human body for validation purposes. It is also recommended that the etching of the antenna during development be done without using acidic etchants as this was found to have significant impact in altering the chemical structure of the FR4 substrate thereby affecting the results. A 3D printing of the antenna board is recommended for further works. Also it is hereby recommended that efforts should be made towards producing hybrid materials for the substrate from simulated materials for better efficiency and improved results.

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