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# A Comprehensive Review of CO2 Capture and Separation Methods

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### ABSTRACT

As the global demand for energy continues to grow rapidly, the use of fossil fuels in power plants is leading to an increase in CO2 emissions. In order to meet the climate change target set at the 21st Conference of the Parties (COP 21), effective strategies are necessary to reduce industrial emissions. One of the most promising methods for accomplishing this is carbon capture and storage (CCS), which involves capturing and separating CO2 generated in thermal power plants. This review explores different approaches and recent advancements in CO2 capture and separation techniques. Carbon capture can be divided into two main categories based on whether CO2 separation is required in the gas stream. The study compares novel methods like oxy-combustion and chemical looping combustion with traditional post-combustion and pre-combustion carbon capture methods. It also examines the current state of technology, limitations associated with each approach, and commonly used techniques for separating CO2 from gas mixtures. The review suggests further research and investigation to improve the capture system, considering factors such as technological maturity, economic viability, and the need for a better understanding of combustion systems.

Keywords: CO2 capture; clean energy technologies; emission reduction; allam cycle; post-combustion; pre-combustion; flue gas treatment

## 1. INTRODUCTION

The rapid growth of industrialization in the past century has resulted in a significant demand for power. The most common method of power generation involves the use of fossil fuels, which leads to the emission of CO2, a major greenhouse gas component. In fact, approximately 65% of GHG emissions come from different power industries and the fossil fuel-based energy sector [1]. Given the increasing global concerns about climate change caused by GHGs, there is a pressing need for research focused on reducing these emissions. Meeting the goals set at the COP-21 agreement, held in Paris in 2015, requires substantial reductions in CO2 emissions to keep the global average temperature rise below 2°C, with efforts aimed at limiting it to 1.5°C [2]. To address emissions, research efforts are underway to explore the use of renewable resources as alternatives to fossil fuels. One interesting approach involves converting CO2 into organic compounds through photocatalytic reduction, enabling the production of renewable fuel feedstock. This process allows for the utilization of traditional fossil fuels as renewable energy sources. For example, Zhou et al. [3] demonstrated the use of the semiconductor ZnS for photocatalytic reduction of CO2 to formate (HCOO-), while Sharma et al. [4] utilized sulfide-based photocatalysts, such as CU3SnS4, for the reduction of CO2 to CH4. Although these methods show promise, no technology has fully replaced conventional fuels yet. While nuclear and renewable energy sources are expected to play a significant role in low-carbon power generation, safety, and other concerns limit their complete substitution for fossil fuels [5]. Therefore, it remains essential to find ways to use conventional fuels for power generation while reducing CO2 emissions. One solution that offers the potential for reducing emissions is Carbon Capture and Storage (CCS) technology. This process involves capturing CO2 emitted from power plants and storing it in a secure location to prevent its release into the environment. The International Energy Agency (IEA) has projected that CCS should contribute to 17% of CO2 abatement by 2035, ensuring cost-effectiveness [6]. To achieve this goal, ongoing research efforts worldwide are focused on developing new technologies. However, the primary challenge for the widespread adoption of CCS is its high cost, which increases electricity prices. Currently, the estimated cost of capturing CO2 using established technologies is at least \$60 per metric ton of CO2, making CCS economically unattractive. This high cost discourages investments in the energy market. Consequently, researchers in developed countries are striving to reduce the cost of carbon capture to around \$20 per metric ton of CO2 [6]. Furthermore, it is crucial to consider the environmental impact of these methods, as reducing CO2 emissions may inadvertently lead to increased emissions of other pollutants that can affect the environment [7]. In terms of carbon capture technologies, there are two main categories: those that involve separation of CO2 and those that do not. This review focuses on examining these processes, assessing the current state of carbon capture technologies, and identifying areas that require further research.

## 2. CARBON CAPTURE WITH SEPARATION

The process of separating CO2 from a gas mixture is a critical requirement in this context and can occur either prior to or following combustion. In the case where the gas stream, containing carbon dioxide, is formed before combustion, it is referred to as precombustion carbon capture. In such instances, the gas stream primarily consists of CO2 and H2. Conversely, if the gas stream is formed after combustion, it is known as post-combustion carbon capture,

with CO2 and N2 being the main constituents. Numerous technologies are currently employed or being developed to separate CO2 from gas mixtures, and these separation techniques are generally applicable to both precombustion and post-combustion processes.

#### 2.1 PRECOMBUSTION CARBON CAPTURE

This method presents an alternative to directly combusting fuel in a combustor [8]. It involves converting the fuel into a combustible gas, which is then used for power generation. Before combustion, CO2 is separated and stored from the gas generated by fossil fuels [9]. A schematic diagram of the process is illustrated in Figure 1 [10].





Initially, synthesis gas (syngas), which is primarily a mixture of H2 and CO with a trace of CO2, is produced from fossil fuel. This can be achieved through steam reforming by adding steam to the fuel [11]. Another method is supplying pure oxygen after separating it from the air and introducing it to the fuel, known as partial oxidation for liquid or gaseous fuels and gasification for solid fuels [11]. The reactions for these processes are as follows [11]:

Steam reforming:  $CxHy + xH2O \rightarrow xCO + (x + y/2) H2$ 

Partial oxidation:  $CxHy + xO2 \rightarrow xCO + (y/2) H2$ 

The syngas produced is then converted from CO to CO2 through a water-gas shift reaction [11]:

 $\rm CO + H2O \rightarrow \rm CO2 + H2$ 

The products of the water-gas shift reaction remain under high pressure, facilitating the removal of CO2 at ambient temperature. The remaining gas consists mainly of hydrogen with minimal impurities and is used to generate power in a combined cycle power plant. The high pressure (typically 2-7 MPa) and high concentration of CO2 (15-60% by volume) before the CO2/H2 separation stage result in lower energy requirements for CO2 separation and compression compared to post-combustion carbon capture [6]. To mitigate the energy penalty caused by air separation and reforming or gasification processes, Sorption Enhanced Water Gas Shift (SEWGS) technology can be employed, integrating the water-gas shift reaction and CO2 separation [12]. SEWGS increases the conversion rate of CO by removing CO2 from the product of the water-gas shift reaction, resulting in additional CO2 emission reduction [13]. While the process is similar for any fossil fuel, using fuels other than natural gas requires additional refining stages to address higher contaminant production [11]. Currently, the main research focus of precombustion carbon capture is on implementing this method in Integrated Gasification Combined Cycle (IGCC) power plants. An IGCC layout is shown in Figure 2. Oxygen is separated from air in a cryogenic air separation plant [14]. The oxygen is then passed to a gasifier where coal is gasified at high pressure and temperature, producing syngas. After cooling and preliminary cleaning, the syngas undergoes a water-gas shift reaction in a water-gas reactor, converting it to H2S, H2, and CO2. Several cleaning steps follow to remove sulfur, mercury, water, and other impurities, resulting in syngas consisting mainly of CO2 and H2. The CO2 is then captured, and the hydrogen is used for power generation. Physical solvents are commonly used for CO2 separation from syngas in commercially developed technologies.

#### 2.2 POST-COMBUSTION CARBON CAPTURE

This technique allows for the capture of CO2 in existing power plants without requiring significant modifications to the plant. This gives it an advantage over other CCS (Carbon Capture and Storage) processes in terms of easier retrofitting [28-30]. It is considered the simplest method for capturing CO2, involving the removal of CO2 from the exhaust flue gases of power plants. Typically, these flue gases exit at atmospheric pressure and contain a relatively low concentration of CO2, as indicated in Table 1. The low concentration of CO2 poses a challenge because the driving force for capture is insufficient [31]. To handle the large volume of flue gases, large-sized equipment, and high capital costs are necessary. Therefore, identifying a cost-effective approach

to capture CO2 from flue gas is crucial.	Additionally, the flue gas	contains various con	ntaminants such as SOx,	NOx, and fly ash,	which further increa	se
the cost of separation using existing tech	nnologies [32].					

Method	Concentration of CO2 (Vol. %)		
Coal-fired Boiler	14		
Natural gas-fired boiler	8		
Natural gas combined cycle	4		
Natural gas partial oxidation	40		
Coal oxygen combustion	>80		

#### Table 1. Amount of CO2 in flue gases of power plants [31].

Separating CO2 from flue gas presents several challenges. Equipment must be designed to withstand the high temperature of the flue gas, and the gas needs to be cleaned before CO2 separation can occur.



Figure 2. Schematic diagram of a simplified flue gas cleanup process for post-combustion carbon capture [32].

Merkel et al. [32] proposed a flow process to clean up the gas, as illustrated in Figure 2. The hot exhaust gas from the boiler undergoes treatment in an electrostatic precipitator (ESP) to remove large particulates. Then, a flue gas desulfurization unit (FGD) removes sulfur products. Post-combustion carbon capture technology is designed to treat the outlet gas from the FGD. At this stage, the gas mixture contains approximately 10-14% CO2, predominantly mixed with nitrogen. Figure 4 depicts a schematic of a coal-fired power plant utilizing solvent-based absorption post-combustion carbon capture. In this setup, coal is pulverized and combusted with air to generate heat. The heat is used to produce steam, which, in turn, drives three different steam turbines operating at various pressures. The low-quality exhaust steam is condensed in a condenser and returned to the boiler. The exhaust flue gas from the boiler goes through a cleaning process to remove sulfur, ash, NOx, and other impurities. After the final stage of cleaning, the gas is directed to the CO2 capture process. When natural gas is used as fuel, the complexity of the system is significantly reduced. Figure 5 illustrates a typical layout of a post-combustion carbon capture is expanded through a gas turbine to generate power. The exhaust from the gas turbine remains at a high temperature, which is utilized to produce steam for additional power generation through a steam turbine. The cooled flue gas then enters the CO2 capture process. Figure 5 depicts a solvent-based CO2 capture system using MEA (Monoethanolamine). MEA scrubbing removes CO2 from the flue gas in the absorber column, leaving clean gas for exhaust. The MEA is subsequently purified in the stripper column for reuse in the absorber column. CO2 is captured from the stripper column and compressed for storage. MEA is the most commonly used method for separating CO2 from flue gas, although other technologies are also employed for this purpose.

## 2.3 CO2 SEPARATION TECHNOLOGY

Numerous separation technologies exist for the separation of CO2 from gas mixtures, and these technologies can be broadly categorized into five sectors: absorption, adsorption, clathrate hydrate process, membrane technology, and calcium looping carbon capture [10]. In the absorption process, research is primarily focused on the development and enhancement of various solvents to improve their performance in capturing CO2. Different solvent systems, such as aqueous amine solutions like monoethanolamine (MEA) and advanced solvents like ammonia-based systems, are being studied to increase their CO2 absorption capacity and selectivity. Additionally, efforts are being made to optimize the operating conditions and improve the energy efficiency of absorption processes. Adsorption technology emphasizes the exploration of new materials and the modification of existing ones to enhance their CO2 adsorption capabilities. Researchers are investigating novel adsorbents, including metal-organic frameworks (MOFs), zeolites, and activated carbon, with tailored properties to selectively capture CO2 from gas mixtures. The focus is on improving the adsorption capacity, kinetics, and stability of these materials to make them more efficient and economically viable. The clathrate hydrate separation process involves the formation of hydrate crystals with

CO2 molecules entrapped within a lattice structure. Research in this area is focused on exploring different thermodynamic promoters and additives to enhance the formation and stability of CO2 hydrates. By optimizing the operating conditions and understanding the kinetics of hydrate formation and dissociation, scientists aim to improve the efficiency of this separation process. Membrane technology utilizes selectively permeable membranes to separate CO2 from gas mixtures based on differences in molecular size, solubility, or diffusion rates. Ongoing research involves the development of advanced membrane materials, such as polymer membranes, mixed matrix membranes, and ceramic membranes, with improved CO2 separation performance. Efforts are also being made to enhance membrane stability, selectivity, and permeability for better process efficiency. Calcium looping carbon capture is a promising technology that utilizes calcium oxide (CaO) as a sorbent to capture CO2 from gas streams. The process involves the cyclic reaction between CaO and CO2 to form calcium carbonate (CaCO3), which can be subsequently calcined to release pure CO2. Researchers are focusing on optimizing the reaction conditions, sorbent properties, and reactor designs to enhance the carbon capture capacity, sorbent stability, and overall process efficiency. Research and development in these five sectors are crucial for advancing CO2 separation technologies and improving their performance in terms of efficiency, selectivity, and cost-effectiveness. Continued efforts in these areas are essential for enabling large-scale deployment of carbon capture and storage (CCS) technologies to mitigate greenhouse gas emissions.

#### 2.4 ABSORPTION

The method of using solvents to absorb CO2 and separate it from a gas stream has been employed on an industrial scale for over 50 years [48]. This absorption process can be classified into two types: physical absorption and chemical absorption, as shown in **Figure 6**. In chemical absorption, the solvent reacts with CO2 to form chemical compounds, which are later separated to obtain pure CO2. In physical absorption, the solvent does not chemically react with CO2 but physically absorbs it. This process is based on Henry's law, which states that the amount of gas dissolved in a solvent is proportional to the gas's partial pressure in equilibrium with the solvent [48].



Figure 3. Classification of absorption processes for CO2 capture [49].

Chemical absorption of CO2 occurs in two stages. In the first stage, the gas stream is brought into contact with the solvent in a counterflow, where CO2 is absorbed by the solvent. The solvent is then regenerated by heating in a stripping column to desorb CO2, which is collected as pure CO2 from the top of the column [10]. The regenerated CO2-lean solvent is recycled back to the absorber [50]. The first stage of the process operates optimally at high pressures and low temperatures, while the second stage performs best at low pressures and high temperatures [10]. Chemical absorption is particularly suitable for capturing CO2 at relatively low pressures, making it advantageous for post-combustion processes that utilize amine or carbonate solvents [48]. In physical absorption, organic or inorganic physical solvents are used that do not chemically react with CO2. This process relies on Henry's law for vapor-liquid equilibrium. Physical absorption shows better performance than chemical absorption at higher partial pressures of CO2, such as in Integrated Gasification Combined Cycle (IGCC) applications [11]. Physical solvents require less energy for regeneration, which is another advantage [52]. However, physical absorption processes have a downside: the solvent's capacity is highest at low temperatures, necessitating cooling of the gas stream prior to absorption, which reduces overall efficiency [52]. Commercially used physical absorption processes include Selexol, Rectisol, and Purisol [11]. A comprehensive comparison using Aspen Plus revealed that Selexol was more energy-efficient for CO2 capture, thanks to its lower energy consumption for solvent regeneration and simpler process [53]. In post-combustion carbon capture, the partial pressure of CO2 in the flue gas stream is typically very low. Therefore, research efforts for this process primarily focus on identifying suitable solvents. Numerous studies have been conducted on different processes and solvents to identify cost-effective absorption methods.



Figure 4. Schematic diagram of a CO2 absorption plant [51].

#### 2.5 ADSORPTION

Adsorption is a separation process that involves removing a component from a mixture using a solid surface. In contrast to absorption processes, adsorption relies on the formation of physical or chemical bonds between the solid adsorbent surface and CO2, driven by intermolecular forces [31]. The adsorption process can absorb single or multiple layers of the gas, depending on factors such as pore size, temperature, pressure, and surface forces [54]. In adsorption, a column is initially filled with the adsorbent material, and the gas stream containing CO2 is passed through the column. CO2 adheres to the solid surface of the adsorbent until the adsorbent becomes saturated. The CO2 is subsequently desorbed from the adsorbent through different cycles to achieve CO2 adsorption [31]. There are four main regeneration cycles used for single-bed CO2 adsorption: pressure swing adsorption (PSA), temperature swing adsorption (TSA), electrical swing adsorption (ESA), and vacuum swing adsorption (VSA). In TSA, the adsorbent's temperature is raised to break the chemical bonds and release CO2. However, this method is costlier due to the additional energy required for heating the adsorbent bed and the time-consuming heating and cooling cycles for regeneration [48]. ESA, on the other hand, utilizes low-voltage electric current to heat the adsorbent rapidly using the Joule effect, enabling fast regeneration. However, ESA requires high-grade electrical energy compared to the low-grade heat energy used in TSA [55]. Pressure swing adsorption involves reducing the pressure of the adsorbent to achieve desorption, while vacuum swing adsorption is a specialized form of PSA used when the feed gas pressure is close to ambient pressure. VSA minimizes the additional energy required for achieving high pressure in PSA by using a partial vacuum downstream of the feed stage to draw the low-pressure feed gas [48]. These cycles can be combined with each other, offering flexibility in the adsorption process. Plaza et al. [56] presented a VSA process model using Aspen Plus for post-combustion carbon capture. A schematic of the regeneration process is shown in Figure 5. Pressure swing operation is advantageous when the partial pressure of CO2 is high, while temperature swing adsorption is more suitable for low CO2 concentrations in the gas stream. PSA becomes less efficient with low CO2 concentrations [58]. Adsorption processes are preferred due to their high adsorption capacity at normal pressure and temperature, long-term stability, low regeneration cost, high adsorption rate, and lower energy requirements [59].



Figure 5. Schematic diagram of different adsorption regeneration cycles: (a) TSA (b) PSA (c) VSA (d)ESA [57].

The focus of research in adsorption processes is finding suitable sorbents to effectively separate CO2 from gas streams. Various substances, such as zeolites, activated carbons, molecular sieves, hydrotalcite, and metal-organic framework materials, have been investigated for this purpose [60]. Garcia et al. demonstrated that the partial pressure of CO2 is a significant factor when using activated carbon as an adsorbent [18]. Sorption-enhanced water gas shift (SEWGS) combines CO2 adsorption with the water gas shift reaction, offering a more economical and energy-efficient alternative to amine scrubbing in absorption processes [61]. Hydrotalcite-based materials are particularly suitable for high-temperature adsorption, showing improved results when used in a sorption-enhanced WGS reactor for enhanced carbon capture [62].

#### 2.6 MEMBRANE TECHNOLOGY

Membranes are barriers made of various materials that selectively separate different substances from mixtures through different mechanisms [31]. They can be composed of organic or inorganic materials and operate based on the solution-diffusion process. In non-facilitated membranes, the permeate, including CO2, dissolves into the membrane and diffuses through it. The amount of CO2 dissolved per unit volume is proportional to the partial pressure of CO2 [63]. Non-facilitated membrane separation technology is particularly useful in pre-combustion capture, where the partial pressure of CO2 is relatively high. Membranes can be utilized in different configurations such as spiral wounds, flat sheets, and hollow fiber modules. They can be selective or non-selective for specific acidic gases [64]. In carbon capture, membrane technology can be classified into two categories: gas separation membranes and gas absorption membranes. In a gas separation membrane system, the gas mixture containing CO2 is introduced at high pressure into a membrane separator, typically consisting of parallel cylindrical membranes. CO2 selectively permeates through the membrane, and it is recovered at a lower pressure on the other side of the membrane. In a gas absorption system, a microporous solid membrane is employed to separate CO2 from the gas stream. Gas absorption systems exhibit high CO2 removal rates due to minimized issues such as flooding, foaming, channeling, and entrainment. Furthermore, the equipment required for gas absorption systems is more compact compared to membrane separators [53]. The two systems are illustrated in Figure 6.



Figure 6. Principle of (a) gas separation membrane and (b) gas absorption membrane

Membrane technology offers several advantages, including the absence of problems such as weeping, entrainment, foaming, and flooding commonly encountered in packed column operations. Membranes also provide a higher surface area and better control of liquid and gas flow rates [65]. However, membranes exhibit reduced effectiveness at lower CO2 concentrations and become impractical when the CO2 concentration in the gas stream falls below 20% [66]. Therefore, they are not well-suited for post-combustion capture processes. One drawback of membranes is their limited lifetime, requiring periodic replacement. Additionally, membrane fibers present higher mass transfer resistance. For optimal performance, membrane pores should be fully occupied by the gas phase. When the liquid phase enters the membrane pores, mass transfer resistance increases, making the membrane economically unjustifiable. This phenomenon is known as membrane wetting. The desired condition is to completely fill the membrane pores with gas, but it is not always achievable. During overextended operational periods, membrane pores can become partially or fully wet [64]. Numerous studies have investigated the effect of wetting on mass transfer through different types of membranes and absorbents. Wetting significantly reduces absorption efficiency, even at low levels. Using ionic liquids as absorbents can improve efficiency by approximately 15% to 20% compared to pure water in counter-current and cocurrent flows [66].

## 2.7 CLATHRATE HYDRATE PROCESS

Gas hydrates or clathrate hydrates, as described in [72], are ice-like crystal compounds formed by water molecules and various substances such as CO2, N2, H2, and O2. These small gas molecules are trapped inside water molecule cavities. The concentrations of gases within the hydrate crystals differ from their original concentrations in the gas mixture [73]. The concept of selectively separating CO2 by forming hydrate crystals between the solid hydrate crystal phase and the gaseous phase is based on thermodynamics. The minimum pressure required to form hydrates at 273.9 K is 5.56 MPa. However, the pressure of syngas after the water gas shift reaction is typically 2-7 MPa, while post-combustion flue gas is close to atmospheric pressure.

Therefore, compressing the gas stream is necessary to enhance hydrate formation rates [74]. The addition of promoters has been studied to reduce the equilibrium conditions for hydrate formation. One extensively studied promoter is tetrahydrofuran (THF), as mentioned in [75]. The equilibrium of hydrate formation decreases with the addition of THF at any temperature. Increasing the THF concentration leads to a decrease in hydrate formation pressure up to an optimum concentration of approximately 1 mol% THF. This allows for CO2 separation without significant compression of flue gas. Moreover, the addition of 3.2 mol% propane to a CO2/O2 mixture can reduce the equilibrium pressure for hydrate formation by 50%, as reported in [76]. For precombustion fuel gas mixtures, the addition of tetra-n-butyl ammonium bromide (TBAB) reduces the hydrate phase equilibrium condition. The hydrate formation condition decreases with an increase in TBAB concentration up to the stoichiometric condition. Beyond that, the phase equilibrium increases with further TBAB concentration [77]. In [78], Park et al. showed that quaternary ammonium salts, including tetrabutylammonium fluoride (TBAF), can capture up to 95% of CO2 from an integrated gasification combined cycle (IGCC) plant using a single step of hydrate formation. TBAF demonstrated better results than TBAB, although with lower gas uptake. Furthermore, recent studies have examined the impact of reactor types. Zheng et al. [79] investigated the effect of bed volume and reactor orientation on hydrate formation in precombustion carbon capture. They found that a horizontal orientation outperformed a vertical configuration. Low water saturation was also found to be preferable for enhancing hydrate formation.

#### 2.8 CALCIUM LOOPING TECHNOLOGY

The calcium looping carbon capture system is an alternative method for capturing CO2 from a gas stream, as described in reference [80]. It involves a direct reaction between CO2 and CaO, resulting in the formation of solid calcium carbonate (CaCO3), which can be easily separated from other gases. The main reversible reaction in this process is:

#### $CaO + CO2 \rightarrow CaCO3$ (1)

The forward reaction, known as the carbonation reaction, is exothermic, while the reverse reaction, called the calcination reaction, is endothermic. The carbonation reaction initially proceeds at a fast rate but eventually slows down [81]. Since the calcination reaction is endothermic, it requires a significant amount of heat supplied at high temperatures. This heat is often generated by the oxy-combustion of coal or natural gas within the calcination reactor [33]. After CO2 is recovered from the calcination reactor, it is compressed and stored. The calcinu looping process can be applied to both precombustion and post-combustion carbon capture. In precombustion carbon capture, the following key reaction occurs in the gasifier:

#### $CO + H2O + CaO \rightarrow CaCO3 + H2$ (2)

Using the calcium looping process in precombustion carbon capture offers advantages such as increasing the destruction rate of tar when hydrogen is used as a fuel and enhancing the conversion rate from CH4 and CO to H2 by removing CO2 from the gas mixture [80]. While the main application of the calcium looping process is in post-combustion carbon capture [82], where limestone captures CO2 from exhaust flue gases in a power plant using a circulating fluidized bed carbonator. The sorbent is then transferred to a calciner operating at higher temperatures. After regeneration, the sorbent is cycled back to the carbonator. The calciner utilizes oxyfuel combustion of coal or natural gas to generate the required heat.



Figure 7. A schematic diagram of post-combustion carbon capture using Calcium looping [82].

## 3. CARBON CAPTURE WITH WATER CONDENSATION

This approach is relatively new in power generation, where pure oxygen is used for combustion instead of supplying air to the combustion chamber. Consequently, the combustion products primarily consist of CO2 and steam. The CO2 in the mixture can be captured by condensing the steam, eliminating the need for separate CO2 separation technologies discussed earlier. As a result, this method is more economically feasible. When oxygen is produced using an Air Separation Unit (ASU), the process is referred to as oxy-combustion carbon capture. Another method of supplying oxygen is through the use of metal oxide in a process called chemical looping combustion [85,86].

#### 3.1. OXY-COMBUSTION CARBON CAPTURE

In this method, the fuel is burned using nearly pure oxygen instead of air. The resulting flue gas consists primarily of a mixture of water and carbon dioxide. In a conventional power plant, fuel is combusted in the presence of air, and the nitrogen in the air acts as a temperature moderator. However, in oxyfuel combustion, since there is no nitrogen present in the combustor, the flame temperature can become excessively high. To control the temperature within the desired range, recycled CO2 is introduced into the combustor along with pure oxygen. Another approach to regulating the flame temperature is by injecting steam into the combustion chamber [87]. After the combustion process, water is separated from the product through condensation. The captured CO2 is then purified and compressed to a supercritical condition for transportation or reuse in the cycle. Figure 8 provides a flow sheet illustrating the concept of oxyfuel combustion.



Figure 8. Flowsheet of oxy-fuel combustion technology for power generation with CO2 capture [5].

Oxy combustion, which involves burning fuel in nearly pure oxygen instead of air, presents different reaction pathways and combustion characteristics compared to conventional air-fuel combustion [88]. Extensive research is required to thoroughly understand and utilize this method due to its unique combustion characteristics. Oxyfuel combustion offers several advantages over conventional combustion methods. In conventional air firing systems, a significant amount of nitrogen is present, which consumes a considerable amount of heat before being released into the environment. However, in oxycombustion, the absence of bulk nitrogen in the combustion environment reduces or eliminates the production of NOx. Moreover, there are no significant pollutants in the combustion products. This makes oxyfuel combustion a more cost-effective method compared to other carbon capture technologies. However, one of the main challenges is the high operational cost associated with producing high-purity oxygen and compressing CO2 after combustion [89]. The production of oxygen with high purity at a reasonable cost remains a major hurdle in oxyfuel combustion. Wu et al. [90] highlighted different research on oxygen separation methods for oxyfuel combustion. They suggested that membrane methods are more economical and simpler compared to cryogenic methods, while adsorption technology is not yet suitable for large-scale implementation. Chemical looping air separation is considered a highly promising and efficient technique for oxyfuel combustion. Ongoing research aims to improve understanding and optimize the oxy-combustion process, including boiler design and a deeper understanding of combustion procedures. Compact boiler designs can reduce the cost of power generation, decrease flue gas volume and associated heat loss, and reduce emissions of SOx and NOx while improving combustibility. Oxy combustion has initially been applied to industrial processes and later explored for CO2 generation for oil recovery. The incorporation of recycled flue gas was subsequently introduced to produce a high-purity CO2 stream for oil recovery and mitigate the environmental impact of fossil fuel power plants [92, 93]. Oxy combustion can be applied to coal and natural gas, classified as oxy-pulverized coal processes, oxy-coal-fired boiler processes, CO2-based cycles, or water-based cycles [94]. Comparisons with other systems have shown that oxy-fuel systems have 1-5% less efficiency loss compared to post-combustion capture, with pressurized systems gaining approximately 3% more efficiency. The ASU may require more power in a pressurized system, but it saves significant power during CO2 compression. The absorptivity and emissivity of flue gases increase in oxyfuel combustion due to higher partial pressures. The ratio of the recycle stream depends on the fuel type, heat recuperator arrangement, and recycling strategy. The oxy-fuel environment has no significant influence on the devolatilization process of solid fuel, but it does result in longer ignition delays compared to conventional systems. Researchers have investigated the effect of recycled CO2 on the combustion environment. The incorporation of CO2 instead of N2 in the combustion environment can decrease the burning velocity or speed of flame propagation [97]. Studies have shown contrasting results regarding the flame speed in an oxy-fuel environment compared to an air-fuel environment, potentially attributed to different experimental setups [97, 98]. Water vapor has also been found to affect flame propagation speed, with an increase in steam concentration leading to a decrease in flame velocity [99]. The presence of CO2 in the oxyfuel environment strengthens the radiation effect of CH4, and the maximum flame temperature is influenced by factors such as the presence of CO2, H2O, and pressure [88, 101]. Limited research has been conducted on ignition, flame stability, and flame extinction in an oxy-combustion environment. Ignition delay is typically longer in an oxy-fuel environment due to the participation of CO2 in chemical reactions, higher heat capacity, and different collision efficiency [102, 103]. The flammability of oxy-methane flames is also influenced by the addition of CO2 and steam, affecting the upper and lower flammability limits [104]. A novel approach to power generation, known as the Allam cycle, has been proposed by Allam et al. [107]. This cycle utilizes oxyfuel combustion and operates with pressurized supercritical CO2 as the working fluid. The key advantage of the Allam cycle lies in the high heat capacity of high-pressure CO2 compared to low-pressure CO2, eliminating the need for water vaporization and condensation in the cycle. In the Allam cycle, fuel is burned in pure oxygen in a high-pressure combustor, generating a feed stream with pressures ranging from 200 to 400 bar. This stream is expanded in a single turbine with a pressure ratio of 6 to 12. The heat from the high-temperature turbine exhaust is transferred to a high-pressure recycled CO2 stream in a recuperator. The recycled stream is then sent back to the combustor to control the turbine inlet temperature. The authors reported theoretical thermal efficiencies of 59% for natural gas fuel and 52% for coal fuel, while inherently capturing CO2. A 50 MWth demonstration plant utilizing the Allam cycle with natural gas as fuel has been recently completed in La Porte, Texas, and plans are underway for a commercial 300 MW plant to showcase the advantages of this cycle [114]. As CO2 capture is integrated within the cycle, no additional measures are required, making it a potentially cost-effective alternative to conventional power plants employing CCS. Ongoing research aims to optimize the parameters of the Allam cycle. Key factors affecting its efficiency include turbine inlet temperature and pressure, turbine outlet pressure, temperature difference on the hot side of the primary heat exchanger, and the performance of the air separation unit within the cycle.



Figure 9. Schematic of the Allam power cycle operating on natural gas as fuel [107].

### 4. COMPARISON OF THE METHODS

Carbon capture processes that require the separation of CO2 have been developed over time and have reached a certain level of maturity, with established full-scale applications. Numerous experimental and numerical modeling studies have been conducted on these processes. One advantage of postcombustion capture is its easy integration with existing power plants. However, the concentration and partial pressure of CO2 in flue gases are typically low, necessitating additional energy and costs to achieve the minimum required concentration for transportation and storage. Chemical absorption processes for separation can lead to solvent degradation and severe corrosion of equipment, resulting in high costs for solvents and equipment, increasing the cost of electricity production by around 70% [118]. Research is ongoing to develop new solvents and reduce the cost of carbon capture. The large size of the equipment also contributes to high capital and operating costs in this method. Pre-combustion carbon capture is predominantly used in process industries, and there are full-scale CCS plants in some industries that utilize this method [11]. The gas mixture in this process contains a higher amount of CO2 compared to conventional flue gas mixtures. Due to the higher pressure and lower gas volume, less energy is required in pre-combustion capture. It is mainly used in integrated gasification combustion capture. However, there is still a significant energy penalty associated with pre-combustion capture. It is mainly used in integrated gasification combined cycle (IGCC) technology, which requires a large auxiliary system, leading to high capital costs compared to other systems.

On the other hand, carbon capture processes that do not require separation are relatively new in power generation, and there are no full-scale operational plants based on these processes. Some pilot-scale operations and subscale demonstration plants are under development, particularly using oxyfuel combustion [10, 30, 94]. One promising example is the 50 MWth demonstration power plant built in Texas by Net Power using the Allam cycle concept, aiming for near-zero emissions. This method offers advantages such as equipment size reduction, compatibility with various types of coal, and no need for an onsite chemical plant. However, it requires a large amount of high-purity oxygen, necessitating an energy-intensive Air Separation Unit (ASU) for oxygen production. Membrane-based technology for air separation may offer competition to cryogenic ASU through greater integration into the power

cycle [133]. The ASU and CO2 compression units used in this process significantly decrease net power output. Furthermore, there are technical uncertainties that require further research to understand full-scale operation. Nonetheless, since no additional cost is required for CO2 separation, this process remains promising for low-cost electricity production while achieving near-zero emissions. The process of Calcium Looping Combustion (CLC) for carbon capture is still in the preliminary stage and has not been implemented commercially. Further research is needed to fully harness its potential. One advantage of CLC is the absence of flame, resulting in no thermal NOx production, and the outlet stream from the air reactor is environmentally benign [93]. Developing appropriate oxygen carriers for CLC could make it more attractive compared to other processes. Bituminous coal is considered for coal-based power plants due to its extensive use in power production [30]. The Selexol process is considered for pre-combustion carbon capture in an IGCC GE-type gasifier. For chemical looping combustion, ilmenite and nickel aluminum oxide were used as oxygen carriers for coal-based and natural gas-based power production, respectively [134, 135]. When coal is used as a fuel, the CLC exhibits the same efficiency as the base combustion technology using pulverized coal without any capture. Reduction in efficiency is the highest in pre-combustion carbon capture. Post-combustion and oxy-combustion carbon capture show an almost similar drop in efficiency. An interesting observation in this comparison is the efficiency of the Allam cycle [30]. When natural gas is used as fuel, the pre-combustion carbon capture shows a 14% drop in the efficiency from the reference powerplant whereas the postcombustion carbon capture shows an 8% drop. The traditional oxy-combustion process exhibits an efficiency of 44.7%. Chemical looping combustion indicates only a 4% drop in efficiency from the reference plant. The Allam cycle shows an extraordinary performance whose efficiency happens to be over 3 percentage points higher than that of the reference combined cycle without CO2 capture [30]. From the efficiency comparison of, it may be concluded that the chemical looping combustion and the Allam cycle are expected to be the leading technologies in the near future for fossil fuel-based power generation. The 50 MWth Allam cycle provides the basis for the deployment of large-scale facilities. Currently, 300 MW natural gas-fired plants are under development. The chemical looping method is not yet technologically ready to implement on an industrial basis. The method is still in the investigation stage. More experimental data are necessary before large-scale commercialization [134,135]. Conventional carbon capture process results in a reduction of efficiency. More fuel is burnt per unit of electricity production due to this inefficiency which leads to more production of CO2. Also, the processes used for capturing carbon dioxide may affect the environment in different ways other than direct emission of CO2. For example, different substances used for separating and capturing CO2 may have undesired effects on the human body and environment. Using a solid sorbent covered with coating was experimented with to reduce the formation of dust from the substance [136]. This could also reduce the capacity of the substance to capture carbon dioxide. Also, stripping of organic solvent from membranes and sorbents is suggested to prevent undesired odor. Before employing carbon capture, it should be ensured that reducing CO2 is not being achieved at the cost of other environmental impacts. Life cycle assessment of the plants is necessary to properly understand the environmental impacts of the carbon capture methods [7,137,138,139,140,141]. Schreiber et al. [7] used the life cycle assessment (LCA) methodology for post-combustion carbon capture using MEA whose impact on the environment and human health was investigated for five power plants. The global warming potential (GWP), human toxicity potential (HTP), acidification potential (AP), photo oxidant formation potential, and eutrophication potential (EP) were considered as impact categories. As expected, GWP was much lower with MEA compared to the power plants without capture whereas HTP was three times higher with MEA plants. Schreiber et al. [7] concluded that upstream and downstream processes such as emissions from fuel and material supply, waste disposal, and wastewater treatment influence the environmental impact measures for power plants with carbon capture. Viebahn et al. [137] revealed about a 40% increase in AP, EP, and HTP when post-combustion carbon capture was implemented in a power plant. A similar result was found by Veltman et al. [138]. They showed that a power plant with post-combustion capture yields a 10 times increase in toxic impacts on freshwater compared to a plant without capture. Impacts on other categories were negligible. Degradation of MEA resulted in the emission of ammonia, acetaldehyde, and formaldehyde. Cuellar et al. [139] compared the life cycle environmental impacts of carbon capture and storage with carbon capture and utilization. GWP with utilization was much greater than that with storage. The highest reduction of GWP was found for pulverized coal and IGCC plants employing the oxyfuel capture method as well as combined cycle gas turbine plants equipped with a post-combustion capture technology. Pehnt et al. [140] showed that a conventional power plant operating on coal with post-combustion carbon capture would result in an increase in the environmental impact in almost all categories except GWP. Solvent degradation and energy penalty due to the CO2 capture process are the main reasons for this increase. Precombustion capture showed a decrease in all the environmental impact categories compared to a conventional power plant. They identified oxyfuel combustion as the most potential process to reduce all the environmental impact categories if co-capture of other pollutants can be achieved.Nie et al. [141] investigated the comparative environmental impacts of post-combustion and oxy-fuel combustion carbon capture. Their analysis showed that almost all environmental impact categories except GWP would increase with post-combustion carbon capture. The same is true for oxyfuel combustion except for GWP, AP, and EP. However, the amount of increase of these impact categories was found to be less in oxyfuel combustion compared to the post-combustion carbon capture. No LCA analysis was found for chemical looping combustion and the newly proposed Allam cycle based on oxyfuel technology.

#### **5. CONCLUSION**

Despite the adverse environmental impact of fossil fuels, they continue to dominate the power generation sector. This review provides a comprehensive discussion of various technologies aimed at reducing emissions from fossil fuel sources. Retrofitting existing power plants with post-combustion carbon capture technology, which involves separating CO2, is considered the most suitable option. Integrated gasification combined cycle (IGCC) plants are well-suited for pre-combustion carbon capture. Post-combustion carbon capture can be implemented without extensive modifications to operational power plants. The separation of CO2 from the gas stream in these processes requires additional energy, resulting in increased electricity prices. Different technologies are available for CO2 separation, with pre-combustion processes being less costly due to the higher partial pressure of CO2. The absorption processes is limited by low CO2 adsorption capacity and gas influence on adsorbents. The development of new adsorbents is necessary to overcome these limitations. Membrane technology offers lower energy consumption but is less effective at low CO2 concentrations. Further research is needed to

understand membrane behavior at higher capacities. Clathrate hydrate formation shows promise for CO2 separation, but the development of suitable additives or promoters is required to enhance competitiveness. Carbon capture with water condensation is economically viable due to simpler design, higher plant efficiency, and favorable life cycle environmental aspects compared to other capture methods. Life cycle assessments demonstrate that oxyfuel combustion has a smaller environmental impact compared to other methods. However, further research is required to fully understand the unique combustion characteristics and optimize its competitiveness. Oxyfuel combustion-based near-zero emission power cycles, such as the Allam cycle, require additional research and experimental data for validation. Chemical looping combustion is a promising technology for emissions reduction, but the availability of suitable oxygen carriers and proper reactor design are critical for its success. Life cycle assessments of these new methods are also necessary to assess their environmental impact accurately. Continued research and development in these areas are essential to address the challenge of global climate change effectively.

#### 6. REFERENCES

1. United States Environmental Protection Agency (EPA)

2. Global Greenhouse Gas Emissions Data

3. Rogelj, J.; Den Elzen, M.; Höhne, N.; Fransen, T.; Fekete, H.; Winkler, H.; Schaeffer, R.; Sha, F.; Riahi, K.; Meinshausen, M.

4. Paris Agreement climate proposals

5. Zhou, R.; Guzman, M.I. CO2 reduction under periodic illumination of ZnS.

6. Sharma, N.; Das, T.; Kumar, S.; Bhosale, R.; Kabir, M.; Ogale, S. Photocatalytic activation and reduction of CO2 to CH4 over single phase nano Cu3SnS4: A combined experimental and theoretical study.

7. Wall, T.; Liu, Y.; Spero, C.; Elliott, L.; Khare, S.; Rathnam, R.; Zeenathal, F.; Moghtaderi, B.; Buhre, B.; Changdong, S.; et al. An overview on oxyfuel coal combustion-state of the art research and technology development.

8. Lockwood, T. A comparative review of next-generation carbon capture technologies for coal-fired power plant.

9. Schreiber, A.; Zapp, P.; Kuckshinrichs, W. Environmental assessment of German electricity generation from coal-fired power plants with amine-based carbon capture.

10. Pardemann, R.; Meyer, B. Pre-Combustion carbon capture.

11. Babu, P.; Ong, H.W.N.; Linga, P. A systematic kinetic study to evaluate the effect of tetrahydrofuran on the clathrate process for pre-combustion capture of carbon dioxide.

12. Theo, W.L.; Lim, J.S.; Hashim, H.; Mustaffa, A.A.; Ho, W.S. Review of pre-combustion capture and ionic liquid in carbon capture and storage.

13. Jansen, D.; Gazzani, M.; Manzolini, G.; van Dijk, E.; Carbo, M. Pre-Combustion CO2 capture.

14. Gazzani, M.; Macchi, E.; Manzolini, G. CO2 capture in natural gas combined cycle with SEWGS. Part A: Thermodynamic performances.

15. Gazzani, M.; Macchi, E.; Manzolini, G. CO2 capture in integrated gasification combined cycle with SEWGS—Part A: Thermodynamic performances.

16. Davies, K.; Malik, A.; Li, J.; Aung, T.N. A meta-study on the feasibility of the implementation of new clean coal technologies to existing coal-fired power plants in an effort to decrease carbon emissions.

17. Romano, M.C.; Chiesa, P.; Lozza, G. Pre-Combustion CO2 capture from natural gas power plants, with ATR and MDEA processes.

18. Martin, C.; Stockel, E.; Lowes, C.R.; Adams, D.; Cooper, A.; Pis, J.; Rubiera, F.; Piveda, C. Hypercrosslinked organic polymer networks as potential adsorbents for pre-combustion CO2 capture.

19. Schell, J.; Casas, N.; Blom, R.; Spjelkavik, A.I.; Andersen, A.; Cavka, J.H.; Mazzotti, M. MCM-41, MOF and UiO-67/MCM-41 adsorbents for precombustion CO2 capture by PSA: Adsorption equilibria.

20. Moioli, S.; Giuffrida, A.; Gamba, S.; Romano, M.C.; Pellegrini, L.; Lozza, G. Pre-Combustion CO2 capture by MDEA process in IGCC based on air-blown gasification.

21. Jiang, G.; Huang, Q.; Kenarsari, S.D.; Hu, X.; Russell, A.G.; Fan, M.; Shen, X. A new mesoporous amine-TiO2 based pre-combustion CO2 capture technology.

22. Park, S.H.; Lee, S.J.; Lee, J.W.; Chun, S.N.; Lee, J.B. The quantitative evaluation of two-stage pre-combustion CO2 capture processes using the physical solvents with various design parameters.

23. Dai, Z.; Deng, L. Membrane absorption using ionic liquid for pre-combustion CO2 capture at elevated pressure and temperature.

24. Yang, M.; Jing, W.; Zhao, J.; Ling, Z.; Song, Y. Promotion of hydrate-based CO2 capture from flue gas by additive mixtures (THF + TBAB).

25. Zheng, J.; Zhang, P.; Linga, P. Semiclathrate hydrate process for pre-combustion capture of CO2 at near ambient temperatures.

26. Usman, M.; Hillestad, M.; Deng, L. Assessment of a membrane contactor process for pre-combustion CO2 capture by modeling and integrated process simulation.

27. Zhai, H.; Rubin, E.S. Systems analysis of physical absorption of CO2 in ionic liquids for pre-combustion carbon capture.

28. Hammond, G.P.; Spargo, J. The prospects for coal-fired power plants with carbon capture and storage: A UK perspective.

29. Yoro, K.; Sekoai, P. The potential of CO2 capture and storage technology in South Africa's coal-fired thermal power plants.

30. Leung, D.Y.C.; Caramanna, G.; Maroto-Valer, M.M. An overview of the current status of carbon dioxide capture and storage technologies.

31. Mondal, M.K.; Balsora, H.K.; Varshney, P. Progress and trends in CO2 capture/separation technologies: A review.

32. Merkel, T.C.; Lin, H.; Wei, X.; Baker, R. Power plant post-combustion carbon dioxide capture: An opportunity for membranes.

33. Adams, T.A., II; Hoseinzade, L.; Madabhushi, P.B.; Okeke, I.J. Comparison of CO2 capture approaches for fossil-based power generation: Review and meta-study.

34. Agarwal, A.; Biegler, L.T.; Zitney, S.E. A superstructure-based optimal synthesis of PSA cycles for post-combustion CO2 capture.

35. Wappel, D.; Gronald, G.; Kalb, R.; Draxler, J. Ionic liquids for post-combustion CO2 absorption.

36. Mason, J.A.; Sumida, K.; Herm, Z.R.; Krishna, R.; Long, J.R. Evaluating metal-organic frameworks for post-combustion carbon dioxide capture via temperature swing adsorption.

37. Savile, C.K.; Lalonde, J.J. Biotechnology for the acceleration of carbon dioxide capture and sequestration.

38. Lee, Z.H.; Lee, K.T.; Bhatia, S.; Mohamed, A.R. Post-combustion carbon dioxide capture: Evolution towards utilization of nanomaterials.

39. Scholes, C.A.; Ho, M.T.; Wiley, D.E.; Stevens, G.W.; Kentish, S.E. Cost competitive membrane-cryogenic post-combustion carbon capture.

40. Bae, T.H.; Hudson, M.R.; Mason, J.A.; Queen, W.L.; Dutton, J.J.; Sumida, K.; Micklash, K.J.; Kaye, S.S.; Brown, C.M.; Long, J.R. Evaluation of cation-exchanged zeolite adsorbents for post-combustion carbon dioxide capture. Apologies for the inconvenience caused. Here is the corrected list:

41. Zhang, Z.; Yan, Y.; Zhang, L.; Chen, Y.; Ju, S. CFD investigation of CO2 capture by methyl diethanolamine and 2-(1-piperazinyl)-ethylamine in membranes: Part B. Effect of membrane properties. J. Nat. Gas Sci. Eng. 2014, 19, 311–316. [CrossRef]

42. Shakerian, F.; Kim, K.H.; Szulejko, J.E.; Park, J.W. A comparative review between amines and ammonia as sorptive media for post-combustion CO2 capture. Appl. Energy 2015, 148, 10–22. [CrossRef]

43. Zhang, Z. Comparisons of various absorbent effects on carbon dioxide capture in membrane gas absorption (MGA) process. J. Nat. Gas Sci. Eng. 2016, 31, 589–595. [CrossRef]

44. El Hadri, N.; Quang, D.V.; Goetheer, E.L.V.; Abu Zahra, M.R.M. Aqueous amine solution characterization for the post-combustion CO2 capture process. Appl. Energy 2017, 185, 1433–1449. [CrossRef]

45. Thompson, J.G.; Combs, M.; Abad, K.; Bhatnagar, S.; Pelgen, J.; Beaudry, M.; Rochelle, G.; Hume, S.; Link, D.; Figueroa, J.; et al. Pilot testing of a heat integrated 0.7 MWe CO2 capture system with two-stage air-stripping: Emission. Int. J. Greene. Gas Control 2017, 64, 267–275. [CrossRef]

46. Thompson, J.G.; Combs, M.; Abad, K.; Bhatnagar, S.; Pelgen, J.; Beaudry, M.; Rochelle, G.; Hume, S.; Link, D.; Figueroa, J.; et al. Pilot testing of a heat integrated 0.7 MWe CO2 capture system with two-stage air-stripping: Amine degradation and metal accumulation. Int. J. Greene. Gas Control 2017, 64, 23–33. [CrossRef]

47. Zhang, Z.; Chen, F.; Rezakazemi, M.; Zhang, W.; Lu, C.; Chang, H.; Quan, X. Modeling of a CO2-piperazine-membrane absorption system. Chem. Eng. Res. Des. 2017, 131, 375–384. [CrossRef]

48. Rackley, S.A. Absorption capture systems. In Carbon Capture and Storage, 2nd ed.; Elsevier: Amsterdam, The Netherlands, 2017.

49. Padurean, A.; Cormos, C.-C.; Agachi, P.-S. Pre-Combustion carbon dioxide capture by gas–liquid absorption for integrated gasification combined cycle power plants. Int. J. Greene. Gas Control 2012, 7, 1–11. [CrossRef]

50. Yu, C.H.; Huang, C.H.; Tan, C.S. A review of CO2 capture by absorption and adsorption. Aerosol Air Qual. Res. 2012, 12, 745–769. [CrossRef]

51. Mofarahi, M.; Khojasteh, Y.; Khaledi, H.; Farahnak, A. Design of CO2 absorption plant for recovery of CO2 from flue gases of the gas turbine. Energy 2008, 33, 1311–1319. [CrossRef]

52. Figueroa, J.D.; Fout, T.; Plasynski, S.; McIlvried, H.; Srivastava, R.D. Advances in CO2 capture technology—The U.S. Department of Energy's Carbon Sequestration Program. Int. J. Greene. Gas Control 2008, 2, 9–20. [CrossRef]

53. Berstad, D.; Anantharaman, R.; Nekså, P. Low-Temperature CCS from an IGCC power plant and comparison with physical solvents. Energy Procedia 2013, 37, 2204–2211. [CrossRef]

54. Meisen, A.; Shuai, X. Research and development issues in CO2 capture. Energy Convers. Manag. 1997, 38, S37-S42. [CrossRef]

55. Lillia, S.; Bonalumi, D.; Grande, C.; Manzolini, G. A comprehensive modeling of the hybrid temperature electric swing adsorption process for CO2 capture. Int. J. Greene. Gas Control 2018, 74

56. Plaza, M.G.; Durán, I.; Rubiera, F.; Pevida, C. Adsorption-Based process modeling for post-combustion CO2 capture. Energy Procedia 2017, 114, 2353–2361. [CrossRef]

57. Songolzadeh, M.; Soleimani, M.; Takht Ravanchi, M.; Songolzadeh, R. Carbon dioxide separation from flue gases: A technological review emphasizing a reduction in greenhouse gas emissions. Sci. World J. 2014, 2014, 828131. [CrossRef] [PubMed]

58. Grande, C.A. Advances in pressure swing adsorption for gas separation. ISRN Chem. Eng. 2012. [CrossRef]

59. Rashidi, N.A.; Yusup, S. An overview of activated carbons utilization for the post-combustion carbon dioxide capture. J. CO2 Util. 2016, 13, 1–16. [CrossRef]

60. Langlois, P.; Pentchev, I.; Hinkov, I.; Lamari, F.D.; Langlois, P.; Dicko, M.; Chilev, C.; Pentchev, I. Carbon dioxide capture by adsorption. J. Chem. Tech. Matall. 2016, 51, 609–627.

61. Wright, A.; White, V.; Hufton, J.; Selow, E.; van Hinderink, P. Reduction in the cost of pre-combustion CO2 capture through advancements in sorption-enhanced water-gas-shift. Energy Procedia 2009, 1, 707–714. [CrossRef]

62. Cobden, P.D.; van Beurden, P.; Reijers, H.T.J.; Elzinga, G.D.; Kluiters, S.C.A.; Dijkstra, J.; van den Brink, R.W. Sorption-Enhanced hydrogen production for pre-combustion CO2 capture: Thermodynamic analysis and experimental results. Int. J. Greenh. Gas Control 2007, 1, 170–179. [CrossRef]

63. Khalilpour, R.; Mumford, K.; Zhai, H.; Abbas, A.; Stevens, G.; Rubin, E.S. Membrane-Based carbon capture from flue gas: A review. J. Clean. Prod. 2015, 103, 286–300. [CrossRef]

64. Ibrahim, M.H.; El-Naas, M.H.; Zhang, Z.; Van der Bruggen, B. CO2 capture using hollow fiber membranes: A review of membrane wetting. Energy Fuels 2018, 32, 963–978. [CrossRef]

65. El-Naas, M.H.; Al-Marzouqi, M.; Marzouk, S.A.; Abdullatif, N. Evaluation of the removal of CO2 using membrane contactors: Membrane wettability. J. Membr. Sci. 2010, 350, 410–416. [CrossRef]

66. Rostami, S.; Keshavarz, P.; Raeissi, S. Experimental study on the effects of an ionic liquid for CO2 capture using hollow fiber membrane contactors. Int. J. Greenh. Gas Control 2018, 69, 1–7. [CrossRef]

67. Kreulen, H.; Smolders, C.A.; Versteeg, G.F.; Van Swaaij, W.P.M. Determination of mass transfer rates in wetted and non-wetted microporous membranes. Chem. Eng. Sci. 1993, 48, 2093–2102. [CrossRef]

68. Mavroudi, M.; Kaldis, S.P.; Sakellaropoulos, G.P. Reduction of CO2 emissions by a membrane contacting process. Fuel 2003, 82, 2153–2159. [CrossRef]

69. Kreulen, H.; Smolders, C.A.; Versteeg, G.F.; van Swaaij, W.P.M. Microporous hollow fiber membrane modules as gas-liquid contactors part 2. Mass transfer with chemical reaction. J. Membr. Sci. 1993, 78, 217–238. [CrossRef]

70. Dindore, V.Y.; Brilman, D.W.F.; Geuzebroek, R.H.; Versteeg, G.F. Membrane-Solvent selection for CO2 removal using membrane gas-liquid contactors. Sep. Purif. Technol. 2004, 40, 133–145. [CrossRef]

71. Malek, A.; Li, K.; Teo, W.K. Modeling of microporous hollow fiber membrane modules operated under partially wetted conditions. Ind. Eng. Chem. Res. 1997, 36, 784–793. [CrossRef]

72. Kumar, R.; Linga, P.; Englezos, P. Pre and Post Combustion Capture of Carbon Dioxide via Hydrate Formation. In Proceedings of the 2006 IEEE EIC Climate Change Technology Conference, EICCCC 2006, Ottawa, ON, Canada, 10–12 May 2006; pp. 1–7.

73. Zhong, D.; Sun, D.; Lu, Y.; Yan, J.; Wang, J. Adsorption—Hydrate hybrid process for methane separation from a CH4/N2/O2 gas mixture using pulverized coal particles. Ind. Eng. Chem. Res. 2014, 53, 15738–15746. [CrossRef]

74. Babu, P.; Linga, P.; Kumar, R.; Englezos, P. A review of the hydrate-based gas separation (HBGS) process for carbon dioxide pre-combustion capture. Energy 2015, 85, 261–279. [CrossRef]

75. Lee, H.J.; Lee, J.D.; Linga, P.; Englezos, P.; Kim, Y.S.; Lee, M.S.; Kim, Y.D. Gas hydrate formation process for pre-combustion capture of carbon dioxide. Energy 2010, 36, 2729–2733. [CrossRef]

76. Kumar, R.; Wu, H.J.; Englezos, P. Incipient hydrate phase equilibrium for gas mixtures containing hydrogen, carbon dioxide, and propane. Fluid Ph. Equilib. 2006, 244, 167–171. [CrossRef]

77. Kim, S.M.; Lee, J.D.; Lee, H.J.; Lee, E.K.; Kim, Y. Gas hydrate formation method to capture the carbon dioxide for pre-combustion process in IGCC plant. Int. J. Hydrog. Energy 2011, 36, 1115–1121. [CrossRef]

78. Park, S.; Lee, S.; Lee, Y.; Seo, Y. CO2 capture from simulated fuel gas mixtures using semi-clathrate hydrates

80. Blamey, J.; Anthony, E.J.; Wang, J.; Fennell, P.S. The calcium looping cycle for large-scale CO2 capture. Prog. Energy Combust. Sci. 2010, 36, 260–279. [CrossRef]

81. Silaban, A.; Harrison, D.P. High temperature capture of carbon dioxide: Characteristics of the reversible reaction between CaO(s) and CO2(g). Chem. Eng. Commun. 1995, 137, 177–190. [CrossRef]

82. Bui, M.; Adjiman, C.S.; Bardow, A.; Anthony, E.J.; Boston, A.; Brown, S.; Fennell, P.S.; Fuss, S.; Galindo, A.; Hackett, L.A.; et al. Carbon capture and storage (CCS): The way forward. Energy Environ. Sci. 2018, 11, 1062–1176. [CrossRef]

83. Hanak, D.P.; Manovic, V. Calcium looping with supercritical CO2 cycle for decarbonization of coal-fired power plant. Energy 2016, 102, 343–353. [CrossRef]

84. Barker, R. The reversibility of the reaction CaCO3  $\rightarrow$  CaO + CO2. J. Chem. Technol. Biotechnol. 1973, 23, 733–742. [CrossRef]

85. Buhre, B.J.P.; Elliott, L.K.; Sheng, C.D.; Gupta, R.P.; Wall, T.F. Oxy-Fuel combustion technology for coal-fired power generation. Prog. Energy Combust. Sci. 2005, 31, 283–307. [CrossRef]

86. Yin, C.; Yan, J. Oxy-Fuel combustion of pulverized fuels: Combustion fundamentals and modeling. Appl. Energy 2016, 162, 742–762. [CrossRef]

87. Seepana, S.; Jayanti, S. Steam-Moderated oxy-fuel combustion. Energy Convers. Manag. 2010, 51, 1981–1988. [CrossRef]

88. Wang, L.; Liu, Z.; Chen, S.; Zheng, C.; Li, J. Physical and chemical effects of CO2 and H2O additives on counterflow diffusion flame burning methane. Energy Fuels 2013, 27, 7602–7611. [CrossRef]

89. Edge, P.; Gharebaghi, M.; Irons, R.; Porter, R.; Porter, R.T.J.; Pourkashanian, M.; Smith, D.; Stephenson, P.; Williams, A. Combustion modeling opportunities and challenges for oxy-coal carbon capture technology. Chem. Eng. Res. Des. 2011, 89, 1470–1493. [CrossRef]

90. Wu, F.; Argyle, M.D.; Dellenback, P.A.; Fan, M. Progress in O2 separation for oxy-fuel combustion—A promising way for cost-effective CO2 capture: A review. Prog. Energy Combust. Sci. 2018, 67, 188–205. [CrossRef]

91. Huang, X.; Guo, J. Opportunities and challenges of oxy-fuel combustion. In Oxy-Fuel Combustion; Elsevier: Amsterdam, The Netherlands, 2018; pp. 1–12.

92. Abraham, B.M.; Asbury, J.G.; Lynch, E.P.; Teotia, A.P.S. Coal-Oxygen process provides CO2 for enhanced recovery. Oil Gas J. 1982, 80(11), 68–75.

93. Adanez, J.; Abad, A.; Garcia-Labiano, F.; Gayan, P.; De Diego, L.F. Progress in chemical-looping combustion and reforming technologies. Prog. Energy Combust. Sci. 2012, 38, 215–282. [CrossRef]

94. Stanger, R.; Wall, T.; Spörl, R.; Paneru, M.; Grathwohl, S.; Weidmann, M.; Scheffknecht, G.; McDonald, D.; Myöhänen, K.; Ritvanen, J.; et al. Oxyfuel combustion for CO2 capture in power plants. Int. J. Greenh. Gas Control 2015, 40, 55–125. [CrossRef]

95. Stanger, R.; Wall, T. Sulphur impacts during pulverized coal combustion in oxy-fuel technology for carbon capture and storage. Prog. Energy Combust. Sci. 2011, 37, 69–88. [CrossRef]

96. Chen, L.; Yong, S.Z.; Ghoniem, A.F. Oxy-Fuel combustion of pulverized coal: Characterization, fundamentals, stabilization, and CFD modeling. Prog. Energy Combust. Sci. 2012, 38, 156–214. [CrossRef]

97. Chen, S. Fundamentals of oxy-fuel combustion. In Oxy-Fuel Combustion; Elsevier: Amsterdam, The Netherlands, 2018; pp. 13-30.

98. Oh, J.; Noh, D. Laminar burning velocity of oxy-methane flames in atmospheric condition. Energy 2012, 45, 669-675. [CrossRef]

99. Mazas, A.N.; Lacoste, D.A.; Schuller, T. Experimental and Numerical Investigation on the Laminar Flame Speed of CH4/O2 Mixtures Diluted with CO2 and H2O. In Proceedings of the ASME Turbo Expo 2010: Power for Land, Sea, Air, Glasgow, UK, 14–18 June 2010; pp. 411–421.

100. Xie, Y.; Wang, J.; Zhang, M.; Gong, J.; Jin, W.; Huang, Z. Experimental and numerical study on laminar flame characteristics of methane oxy-fuel mixtures highly diluted with CO2. Energy Fuels 2013, 27, 6231–6237. [CrossRef]

101. Seepana, S.; Jayanti, S. Flame structure and NO generation in oxy-fuel combustion at high pressures. Energy Convers. Manag. 2009, 50, 1116–1123. [CrossRef]

102. Koroglu, B.; Pryor, O.M.; Lopez, J.; Nash, L.; Vasu, S.S. Shock tube ignition delay times and methane time-histories measurements during excess CO2 diluted Oxy-Methane Combustion. Combust. Flame 2016, 164, 152–163. [CrossRef]

103. Pryor, O.; Barak, S.; Lopez, J.; Ninnemann, E.; Koroglu, B.; Nash, L.; Vasu, S.; Ninnemann, E.; Koroglu, B.; Nash, L.; et al. High pressure shock tube ignition delay time measurements during oxy-methane combustion with high levels of CO2 dilution. J. Energy Resour. Technol. 2017, 139. [CrossRef]

104. Hu, X.; Yu, Q.; Sun, N.; Qin, Q. Experimental study of flammability limits of oxy-methane mixture and calculation based on thermal theory. Int. J. Hydrog. Energy 2014, 39, 9527–9533. [CrossRef]

105. Said, A.; Eloneva, S.; Fogelholm, C.J.; Fagerlund, J.; Nduagu, E.; Zevenhoven, R. Integrated carbon capture and storage for an oxyfuel combustion process by using carbonation of Mg(OH)2 produced from serpentinite rock. Energy Proceedia 2011, 4, 2839–2846. [CrossRef]

106. Riaza, J.; Gil, M.V.; Álvarez, L.; Pevida, C.; Pis, J.J.; Rubiera, F. Oxy-Fuel combustion of coal and biomass blends. Energy 2012, 41, 429–435. [CrossRef]

107. Allam, R.J.; Palmer, M.R.; Brown, G.W.; Fetvedt, J.; Freed, D.; Nomoto, H.; Itoh, M.; Okita, N.; Jones, C. High efficiency and low cost of electricity generation from fossil fuels while eliminating atmospheric emissions, including carbon dioxide. Energy Procedia 2013, 37, 1135–1149. [CrossRef]

108. Leckner, B.; Gómez-Barea, A. Oxy-Fuel combustion in circulating fluidized bed boilers. Appl. Energy 2014, 125, 308-318. [CrossRef]

109. Vellini, M.; Gambini, M. CO2 capture in advanced power plants fed by coal and equipped with OTM. Int. J. Greenh. Gas Control 2015, 36, 144–152. [CrossRef]

110. Scaccabarozzi, R.; Gatti, M.; Martelli, E. Thermodynamic optimization and part-load analysis of the NET power cycle. Energy Procedia 2017, 114, 551–560. [CrossRef]

111. Falkenstein-Smith, R.; Zeng, P.; Ahn, J. Investigation of oxygen transport membrane reactors for oxy-fuel combustion and carbon capture purposes. Proc. Combust. Inst. 2017, 36, 3969–3976. [CrossRef]

112. Climent Barba, F.; Martínez-Denegri Sánchez, G.; Soler, S.B.; Gohari Darabkhani, H.; Anthony, E.J. A technical evaluation, performance analysis and risk assessment of multiple novel oxy-turbine power cycles with complete CO2 capture. J. Clean. Prod. 2016, 133, 971–985. [CrossRef]

113. Seon, B.; Jae, M.; Ho, J.; Seop, T. Influence of a recuperator on the performance of the semi-closed oxy-fuel combustion combined cycle. Appl. Therm. Eng. 2017, 124, 1301–1311.

114. Laumb, J.D.; Holmes, M.J.; Stanislowski, J.J.; Lu, X.; Forrest, B.; McGroddy, M. Supercritical CO2 cycles for power production. Energy Procedia 2017, 114, 573–580. [CrossRef]

115. Allam, R.J.; Martin, S.; Forrest, B.; Fetvedt, J.; Lu, X.; Freed, D.; Brown, G.W.; Sasaki, T.; Itoh, M.; Manning, J. Demonstration of the allam cycle: An update on the development status of a high efficiency supercritical carbon dioxide power process employing full carbon capture. Energy Procedia 2017, 114, 5948–5966. [CrossRef]

116. Mitchell, C.; Avagyan, V.; Chalmers, H.; Lucquiaud, M. An initial assessment of the value of Allam Cycle power plants with liquid oxygen storage in future GB electricity system. Int. J. Greenh. Gas Control 2019, 87, 1–18. [CrossRef]

117. Ferrari, N.; Mancuso, L.; Davison, J.; Chiesa, P.; Martelli, E.; Romano, M.C. Oxy-Turbine for Power Plant with CO2 Capture. Energy Procedia 2017, 114, 471–480. [CrossRef]

118. Zhang, Z.; Borhani, T.N.G.; El-Naas, M.H. Carbon capture. In Exergetic, Energetic and Environmental Dimensions; Elsevier: Amsterdam, The Netherlands, 2017; pp. 997–1016.

119. Yang, H.; Xu, Z.; Fan, M.; Gupta, R.; Slimane, R.B.; Bland, A.E.; Wright, I. Progress in carbon dioxide separation and capture: A review. J. Environ. Sci. 2008, 20, 14–27. [CrossRef]

120. Hossain, M.M.; De Lasa, H.I. Chemical-Looping combustion (CLC) for inherent CO2 separations—A review. Chem. Eng. Sci. 2008, 63, 4433–4451. [CrossRef]

121. Jin, H.; Ishida, M. A new type of coal gas fueled chemical-looping combustion. Fuel 2004, 83, 2411-2417. [CrossRef]

122. Erlach, B.; Schmidt, M.; Tsatsaronis, G. Comparison of carbon capture IGCC with pre-combustion decarbonisation and with chemical-looping combustion. Energy 2011, 36, 3804–3815. [CrossRef]

123. Shimomura, Y. The CO2 wheel: A revolutionary approach to carbon dioxide capture. Modern Power Syst. 2003, 23, 15–17.

124. Quinn, R.; Kitzhoffer, R.J.; Hufton, J.R.; Golden, T.C. A high temperature lithium orthosilicate-based solid absorbent for post combustion CO2 capture. Ind. Eng. Chem. Res. 2012, 51, 9320–9327. [CrossRef]

125. Dahl, I.M.; Bakken, E.; Larring, Y.; Spjelkavik, A.I.; Håkonsen, S.F.; Blom, R. On the development of novel reactor concepts for chemical looping combustion. Energy Procedia 2009, 1, 1513–1519. [CrossRef]

126. Johansson, M.; Mattisson, T.; Lyngfelt, A. Investigation of Mn3O4 with stabilized ZrO2 for chemical-looping combustion. Chem. Eng. Res. Des. 2006. [CrossRef]

127. Li, J.; Zhang, H.; Gao, Z.; Fu, J.; Ao, W.; Dai, J. CO2 capture with chemical looping combustion of gaseous fuels: An overview. Energy Fuels 2017, 31, 3475–3524. [CrossRef]

128. Tang, M.; Xu, L.; Fan, M. Progress in oxygen carrier development of methane-based chemical-looping reforming: A review. Appl. Energy 2015, 151, 143–156. [CrossRef]

129. Lyngfelt, A.; Kronberger, B.; Adanez, J.; Morin, J.X.; Hurst, P. 2005, The Grace Project: Development of Oxygen Carrier Particles for Chemical-Looping Combustion. Design and Operation of a 10 KW Chemical-Looping Combustor. In Proceedings of the 7th International Conference on Greenhouse Gas Control Technologies, Vancouver, BC, Canada, 5 September 2004; pp. 115–123.

130. Johansson, E.; Mattisson, T.; Lyngfelt, A.; Thunman, H. Combustion of syngas and natural gas in a 300 W chemical-looping combustor. Chem. Eng. Res. Des. 2006, 36, 3804–3815. [CrossRef]

131. Naqvi, R.; Bolland, O. Multi-Stage chemical looping combustion (CLC) for combined cycles with CO2 Capture. Int. J. Greenh. Gas Control 2007, 1, 19–30. [CrossRef]

132. Zhu, L.; Jiang, P.; Fan, J. Comparison of carbon capture IGCC with chemical-looping combustion and with calcium-looping process driven by coal for power generation. Chem. Eng. Res. Des. 2015, 104, 110–124. [CrossRef]

133. Pfaff, I.; Kather, A. Comparative thermodynamic analysis and integration issues of CCS steam power plants based on oxy-combustion with cryogenic or membrane-based air separation. Energy Procedia 2009, 1, 495–502. [CrossRef]

134. Naqvi, R.; Wolf, J.; Bolland, O. Part-Load analysis of a chemical looping combustion (CLC) combined cycle with CO2 capture. Energy 2007, 32, 360–370. [CrossRef]

135. Fan, J.; Zhu, L.; Hong, H.; Jiang, Q.; Jin, H. Thermodynamic and environmental performance of in situ gasification of chemical looping combustion for power generation using ilmenite with different coals and comparison with other coal-driven power technologies for CO2 capture. Energy 2017, 119, 1171–1180. [CrossRef]

136. Wilberforce, T.; Baroutaji, A.; Soudan, B.; Al-Alami, A.H.; Olabi, A.G. Outlook of carbon capture technology and challenges. Sci. Total Environ. 2019, 657, 56–72. [CrossRef]

137. Viebahn, P.; Nitsch, J.; Fischedick, M.; Esken, A.; Schüwer, D.; Supersberger, N.; Zuberbühler, U.; Edenhofer, O. Comparison of carbon capture and storage with renewable energy technologies regarding structural, economic, ecological aspects in Germany. Int. J. Greenh. Gas Control 2007, 1, 121–133. [CrossRef]

138. Veltman, K.; Singh, B.; Hertwich, E.G. Human and environmental impact assessment of post-combustion CO2 capture focusing on emissions from amine-based scrubbing solvents to air. Environ. Sci. Technol. 2010, 44, 1496–1502. [CrossRef]

139. Cuéllar-Franca, R.M.; Azapagic, A. Carbon capture, storage and utilization technologies: A critical analysis and comparison of their life cycle environmental impacts. J. CO2 Util. 2015, 9, 82–102. [CrossRef]

140. Pehnt, M.; Henkel, J. Life cycle assessment of carbon dioxide capture and storage from lignite power plants. Int. J. Greenh. Gas Control 2009, 3, 49–66. [CrossRef]

141. Nie, Z.; Korre, A.; Durucan, S. Life cycle modelling and comparative assessment of the environmental impacts of oxy-fuel and post-combustion CO2 capture, transport and injection processes. Energy Procedia 2011, 4, 2510–2517. [CrossRef]