# Planning, Analysis and Design of an Institutional Building 

Krishnan. $S^{a}$, Sindhu Vaardini. $U^{b}$<br>${ }^{a}$ Post Graduate Student, M.E Construction Management, Department of Civil Engineering, Kumaraguru College of Technology, Coimbatore, Tamil Nadu, India.<br>${ }^{b}$ Assistant Professor, M.E Construction Management, Department of Civil Engineering, Kumaraguru College of Technology, Coimbatore,Tamil Nadu, India.<br>DOI: https://doi.org/10.55248/gengpi.234.4.39054


#### Abstract

Any construction project will start with the Planning, Layout of the building or structure followed by design and analysis of the structure which is followed by cost estimation. This project involves the layout, design, analysis, planning and cost estimation of an Institutional building located in Thudiyalur municipal area, Coimbatore. Under this layout of the given site has been prepared. The height of each floor is 3.6 m from floor level to top of the roof slab. It is provided with R.C.C. roof slab supported on R.C.C. frames. The columns are connected with beams at roof level. The main outer walls and cross walls are 230 mm thick brick masonry in cement mortar thickness 0.1 mm . The slab, beams, columns and footing are designed as per IS 456-2000.The design are based on the limit state design method. Imposed and dead loads are only considered for design. The drawings are prepared using AutoCAD. The analysis is done both manually and by using software.


Keywords:Planning, Institutional, Construction.

## 1. Introduction

In this project it was proposed to plan, analyse, design and estimate an Institutional building. The Plot area of the site is 16.7 acres. The College is an engineering college with 5 departments. It consist 5 Identical Blocks. A block is designed and similar way is adopted to all the remaining blocks. The college is located at Thudiyalur, Coimbatore, TamilNadu. The height of each floor is 3.6 m from floor level to roof level. It is provided with R.C.C roof slab supported on R.C.C frames and masonry infills. The columns are connected with the beam at roof level. The main outer wall and cross wall are 230 mm thick brick masonry in CM 1:5. Contour maps, Planning of the building and roads, Layouts of various facilities were obtained, Area calculations, Lift calculations were done. The 2D analysis of the structural elements has been done by substitute frame method, cantilever method and result has been cross-checked by using the STAAD PRO results to find the percentage difference. Slabs, beams, columns and footing has been designed manually with the help of IS $456-2000$, SP-16 and IS 875-1987(Part I, II, III).M25 grade concrete is used for slab and beam and M30 for column and footing. Fe 415 steel has been used for the design of all the structural components. SBC of the soil is considered to be $300 \mathrm{kN} / \mathrm{sq} . \mathrm{m}$.. The cost of construction is arrived by estimating in Microsoft Excel by market and SOR rates. The project planning is done by using Microsoft Project in which time and resources are allocated for individual activity and thus the entire project duration is found out.

### 1.2 Topography

The Topography is used to describe the detailed study of the earth's surface. This includes changes in the surface such as mountains and valleys as well as features such as rivers and roads. A Topographic Survey is a survey that gathers data about the elevation. A typical Topography and Contour layout is shown in Fig 2(a),2(b).


Fig. 2 - (a) Topographic layout of the site; (b) Contour layout of the site

### 1.3 Layout

Layout plan shows the arrangement of all facilities which are required to make the structure more versatile to use. A typical layout plan is shown in Fig 3(a),3(b).


Fig. 3 - (a)Ground and First floor plan; (b) Second and Third floor plan.

## Section

The section shown in Fig 4 shows the height of the floors and the material involved in construction from plain cement concrete to the description of the parapet wall.


Fig. 4 - Section cut along the $X$ axis.

## Soil report recommendations

The primary purpose of our investigation is to obtain data to develop foundation design recommendations for the above work. At, first instance, one borehole was bored at site. Client's representatives selected the locations of borings.

To accomplish these purposes, the following tasks were performed:

1. Detailed soil borings were done up to stratum to explore the sub surface stratigraphy and obtain soil samples for testing. Field and laboratory tests were conducted to evaluate the index and engineering properties of the soils
2. Engineering analysis was performed to develop foundation design information for proposed structure.

Based on the sub-soil condition and possible loads on foundation, the following recommendations for proposed construction of Institutional building (G+4).

- The Isolated / combined footing will be recommended for proposed Structure.
- Foundation depth up to 3.6 m from existing ground level.
- $\quad$ SBC recommended is $300 \mathrm{KN} / \mathrm{m}^{2}$ at 2.2 m depth based on STP- N value conducted inside the boreholes (shear failure and settlement criteria).


## Analysis

2D modelling is done by using Staad pro. The components of the size obtained from basic assumption are modelled and loading of the component i.e., combination of dead load, live load and floor finishes are applied and the model is analyzed.

Here the 2D analysis is carried out for the Critical frame (Fig 5) i.e., the mid frame.
Substitute Frame Method:
Load Calculations:
Self-weight of the beam $=0.3 \times 0.3 \times 25 \times 1.5=3.375 \mathrm{KN} / \mathrm{m}$
Dead Load of slab= $3.66 \times 1 \times 0.15 \times 25=13.725 \mathrm{KN} / \mathrm{m}$
Floor Finishes $=1 \mathrm{KN} / \mathrm{m}$
Live Load $=4 \mathrm{kN} / \mathrm{m}$
Total Load=22.1KN/m


Fig. 5 - Critical frame

Table 1 - Manual and software comparison of results

| Member | Manual | Software | \% variation |
| :---: | :---: | :---: | :---: |
| AB | -23.77 | -25.21 | 6.06 |
| AS | 11.87 | 13.45 | 13.31 |
| AJ | 11.87 | 13.45 | 13.31 |
| BC | -9.33 | -10.23 | 9.65 |
| BA | 26.215 | 28.22 | 7.65 |
| BT | -8.64 | -9.73 | 12.62 |
| BK | -8.64 | -9.73 | 12.62 |
| CD | -38.45 | -40.76 | 6.01 |
| CB | 13.63 | 15.56 | 14.16 |
| CU | 11.99 | 13.73 | 14.51 |
| CL | 11.99 | 13.73 | 14.51 |
| DE | -34.66 | -36.22 | 4.50 |
| DC | 43.129 | 47.88 | 11.02 |
| DV | -4.225 | -4.9 | 15.98 |
| DM | -4.225 | -4.9 | 15.98 |
| EF | -13.11 | -14.23 | 8.54 |
| ED | 27.61 | 34.88 | 26.33 |
| EW | -7.56 | -8.22 | 8.73 |
| EN | -7.56 | -8.22 | 8.73 |
| FG | -31.24 | -34.88 | 11.65 |
| FE | 13.95 | 14.99 | 7.46 |
| FX | 8.68 | 9.89 | 13.94 |
| FO | 8.68 | 9.89 | 13.94 |
| GH | -38.43 | -40.11 | 4.37 |
| GF | -32.85 | -35.76 | 8.86 |
| GY | 0.87 | 1 | 14.94 |
| GP | 0.87 | 1 | 14.94 |
| HI | -34.76 | -35.83 | 3.08 |
| HG | 38.02 | 40.72 | 7.10 |
| HZ | -1.69 | -2.01 | 18.93 |
| HQ | -1.69 | -2.01 | 18.93 |
| IH | 25.89 | 27.89 | 7.72 |
| IA1 | -13.1 | -13.9 | 6.11 |
| IR | -13.1 | -13.9 | 6.11 |
|  |  | Average | 11.24 |

## 2. Details of structural members

Table 2 - Details of slab.

| SLAB NO | LONGER SPAN |  | SMALLER |  | $\begin{aligned} & \text { Longer } \\ & \text { span/ } \\ & \text { smaller } \\ & \text { span } \end{aligned}$ | Type of Slab | Req.Depth of Slab | Provided Depth mm | $\begin{aligned} & \text { Reinforcement } \\ & \text { detalls in } \\ & \text { shorter } \\ & \text { Direction } \end{aligned}$ | Reinforcements detalls in Longer direction | Torsion Reinforce ment Area | Torsion <br> Reinforcemts <br> in Both <br> Direction |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | FEET | INCHES | FEET | INCHES |  |  |  |  |  |  |  |  |
| S1 | 19 | 3 | 14 | 6 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \\ & \hline \end{aligned}$ | 140 | 150 | 10 mm dia bars $@ 200 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 10 \mathrm{~mm} \text { dia bars } \\ & @ 180 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | $\begin{aligned} & 8 \mathrm{~mm} \text { dia @ } \\ & 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ |
| S1a | 19 | 3 | 14 | 9 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars $@ 200 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | $\begin{aligned} & 8 \mathrm{~mm} \mathrm{dia} @ \\ & 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ |
| S2 | 19 | 3 | 17 | 2 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 150 | 150 | 10 mm dia bars <br> @ 280 mm C/C | 10 mm dia bars <br> @ $270 \mathrm{~mm} \mathrm{C/C}$ | $\begin{array}{\|l\|} 1070 \times \\ 1070 \mathrm{~mm} \end{array}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S3 | 19 | 11 | 12 | 0 | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 130 | 150 | 10 mm dia bars @ 280 mm C/C | 10 mm dia bars <br> @ $240 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ |
| S4 | 19 | 11 | 6 | 6 | 3 | One way slab | 80 | 150 | 10 mm dia bars @ $200 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S5 | 15 |  | 14 | 6 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars @ 260 mm C/C | 10 mm dia bars <br> @ $260 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ |
| S5a | 15 |  | 14 | 9 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | $\begin{aligned} & \text { 10mm dia bars } \\ & @ 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{~mm} \text { dia bars } \\ & @ 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C/C}$ |
| S6 | 15 |  | 7 |  | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars $@ 200 \mathrm{~mm} \mathrm{C/C}$ | 11 mm dia bars @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 440 \times 440 \\ & \mathrm{~mm} \end{aligned}$ | $\begin{aligned} & 8 \mathrm{~mm} \text { dia @ } \\ & 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ |
| S7 | 14 | 6 | 14 | 3 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars <br> $@ 260 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars <br> @ $260 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S7a | 14 | 9 | 14 | 3 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars <br> @ $260 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ | 10 mm dia bars <br> (1) $260 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| 58 | 14 | 3 | 7 |  | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars <br> $@ 200 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 440 \times 440 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| 59 | 14 | 6 | 7 |  | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars @ 200 mm C/C | 10 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 440 \times 440 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C/C}$ |
| s9a | 14 | 9 | 7 |  | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars <br> @ $200 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 440 \times 440 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C/C}$ |
| S10 | 7 |  | 7 |  | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars $@ 200 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ | 11 mm dia bars <br> @ $180 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ | $\begin{aligned} & 901 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S11 | 14 | 9 | 7 |  | 2 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 90 | 150 | 10 mm dia bars @ $200 \mathrm{~mm} \mathrm{C/C}$ | 10 mm dia bars @ $180 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 440 \times 440 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S12 | 14 | 9 | 14 | 6 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars @ 260 mm C/C | 10 mm dia bars <br> @ $260 \mathrm{~mm} \mathrm{c} / \mathrm{C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | 8 mm dia @ $290 \mathrm{~mm} \mathrm{C} / \mathrm{C}$ |
| S13 | 14 | 9 | 14 | 9 | 1 | $\begin{aligned} & \text { two way } \\ & \text { slab } \end{aligned}$ | 140 | 150 | 10 mm dia bars @ 260 mm C/C | 10 mm dia bars <br> @ $260 \mathrm{~mm} \mathrm{C/C}$ | $\begin{aligned} & 900 \times 900 \\ & \mathrm{~mm} \end{aligned}$ | $\begin{aligned} & 8 \mathrm{~mm} \text { dia @ } \\ & 290 \mathrm{~mm} \mathrm{C/C} \end{aligned}$ |



Fig. 6 - Footing and Column layout
Table 3 - Details of column

| Column name | Column size | Main reinforcement | Shear reinforcement |
| :--- | :--- | :--- | :--- |
| C 1 | $0.45 \mathrm{~m} \times 0.45 \mathrm{~m}$ | $6 \# 25 \mathrm{~mm}$ diameter | 8 mm diameter @ $300 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| C 2 | $0.4 \mathrm{~m} \times 0.4 \mathrm{~m}$ | $6 \# 25 \mathrm{~mm}$ diameter | 8 mm diameter @ $300 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |

Table 4 - Details of footing

| Footing name | Footing size | Main reinforcement | Distribution reinforcement |
| :--- | :--- | :--- | :--- |


| F1 | $2.5 \mathrm{~m} \times 2.5 \mathrm{~m}$ | 12 mm diameter @ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | 12 mm diameter @ $90 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |
| :--- | :--- | :--- | :--- |
| F2 | $2 \mathrm{~m} \times 2 \mathrm{~m}$ | 12 mm diameter @ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ | 12 mm diameter @ $100 \mathrm{~mm} \mathrm{c} / \mathrm{c}$ |

## Design of lift

(AS Per NBC 2016 Part 8 Sec 5A)

## LIFT CALCULATION:

No of lifts in main block $=2$
No of lifts in other block $=1$ (per block)
No of floors (excluding G.F) $=2$
Lift capacity $=10$ persons
(From table 11)
Lift speed $=1 \mathrm{~m} / \mathrm{s}$
(From table 13)
Rated load $=680 \mathrm{~kg}$
Minimum car size $=1.5 \mathrm{~m} \times 1.5 \mathrm{~m}$
Door adopted center opening power operated door
COPD door width $=0.8 \mathrm{~m}$
From table 15,
Pit depth $=1.5 \mathrm{~m}$
Overhead height $=\mathrm{CH}+1.6 \mathrm{~m}$
Consider car clear inside height $(\mathrm{CH})=2.5 \mathrm{~m}$
Overhead height $=4.1 \mathrm{~m}$
Machine room height $=2.5 \mathrm{~m}$

## Entry of Passengers in Ground floor:

Time required for entry of one passenger when lift is partially empty $=1 \mathrm{sec}$
Lift capacity $=10$ nos
Time of entry of passengers $=10 \times 1=10 \mathrm{sec}$

## Entry of passengers on each floor:

Time required for entry of one passenger when lift is partially empty= 1 sec
Lift capacity/4 (assuming 50\% entry of passengers) $=5$ nos
Time of entry of passengers at each floor $=5 \times 1=5$
Total entry on all floors going up $=5 \times 2=10 \mathrm{sec}$
Total entry on all floors going down $=5 \times 2=10 \mathrm{sec}$
Total entry on going up and down=20 sec

## Exit of passengers on each floor:

Time required for exit of one passenger when lift is partially empty $=0.75$
Lift capacity/4(assuming 50\% entry of passengers) $=5$ Nos
Time for entry of passengers at each floor $=0.75 \times 5=3.75 \mathrm{sec}$
Total exit on all floors going up $=3.75 \times 2=7.5$ secs

Total exit on all floors going down $=3.75 \times 2=7.5$ secs
Total exit on all floors going up and down $=15$ secs

## Exit of passengers on top and bottom floor

Time required for exit of one passenger $=0.75$ secs

Lift capacity=10 nos
Time of exit of passengers $=0.75 \times 10=7.5 \mathrm{sec}$

Time of exit on bottom and top floor=15 sec

Door closing and opening time:
Door opening $\&$ closing time at each floor (Door is power operated central open,
for 6 persons capacity) $=3$ secs
Number of floors (Except GF) $=2$ Nos

Door closing and opening time at $\mathrm{GF}=4$ secs
Total time for opening and closing of doors $=(3 \times 2)+4=10$ secs
Total time for opening and closing of doors going up and down $=10$ secs

## Acceleration periods:

Acceleration period for each cycle $($ Assume $)=1.5 \mathrm{secs}$
No of floors excluding GF $=2$ Nos

Total Time $=1.5 \times 2=3 \operatorname{secs}$

## Deceleration periods:

Deceleration period for each cycle (Assume) $=2 \operatorname{secs}$
No of floors excluding GF $=2 \mathrm{Nos}$

Total Time $=2 \times 2=4 \operatorname{secs}$

## Stopping and levelling periods:

Stopping and levelling periods $=2 \sec ($ assume $)$
No of floors $=2$ nos

Total time $=2 \times 2=4 \mathrm{sec}$

Distance travelled by lift during acceleration or deceleration $=\mathrm{d}=\mathrm{ut}+0.5 \mathrm{ft}^{2}$
$\mathrm{u}=0 \mathrm{~m} / \mathrm{s}$
$\mathrm{T}=1.5 \mathrm{sec}$ per cycle
$F($ for lift speed $1.5 \mathrm{~m} / \mathrm{s})=0.75 \mathrm{~m} / \mathrm{s}^{2}$
Period of full rated speed between stops going up
Distance travelled with full rated speed per floor $=2.15 \mathrm{~m}$
No of floors=2 nos

Total distance travelled with full rated speed $=4.3 \mathrm{~m}$
Full rated velocity $=1 \mathrm{~m} / \mathrm{s}$
Time taken $=4.3 \mathrm{sec}$
Period of full rated speed between stops going down
Distance travelled with full rated speed per floor $=2.15 \mathrm{~m}$
No of floors $=4$ Nos

Total distance travelled with full rated speed $=4.3 \mathrm{~m}$
Full rated velocity $=1 \mathrm{~m} / \mathrm{s}$
Time taken $=4.3 \mathrm{secs}$

Round Trip Time $=$ Total time to discharge full one load of passengers from ground floor to roof floor and coming back to ground floor $=117.1 \mathrm{Sec}$
Number of lifts $=1$
Waiting interval $=$ RTT $/ n$

$$
=117.1 / 1=117.1 \mathrm{Sec}
$$

Average number of passengers carried in a car $(80 \%$ of capacity $)=8$ Nos
Total population $=($ No of floors $\times$ Net usable area per floor $) /$ Population Density

## Determination of handling capacity(cl:6.2.9)

Handling capacity $=(300 \times \mathrm{Qx} 100) /(\mathrm{TxP})$
$\mathrm{H}=$ handling capacity as the percentage of the peak population during 5 min period
$\mathrm{P}=$ total population to be handled during peak time
Net usable area per floor $=104.7$ Sq.m
No. of landings including ground $=3$
Assuming population density 12.5 per person
Probable population $\mathrm{P}=(3 \times 104.7) / 12.5=25.126$ persons
$\mathrm{Q}=$ Average no. of passengers carried in a car $=80 \%$ of capacity $=8$ Nos
$\mathrm{H}=(300 \times 8 \times 100) /(25.128 \times 117.1)=8.15 \%$
Provided 1 number of lifts of speed $1 \mathrm{~m} / \mathrm{s}$.

## 4. Conclusion

The ultimate aim of the project work is to give a practical exposure of the designing work of structures from various cadre of the society. A detailed plan of the Institutional building has been prepared taking into account functionality, utility, economy and feasibility. Planning has been done in accordance with University Grants Commission norms, All India Council for Technical Education norms and National Building Code. Area of the site has been efficiently planned such that effective construction will be ensured. Analysis of the structural members has been successfully done by Substitute frame method and are checked using the results obtained from STAAD Pro software. The structure members have been designed by limit state method. Structural drawings have been prepared with the help of AUTOCAD software. All members are economic sections and safe against failure. The total cost of the institutional building has been estimated to be $\square 8.62$ crores (approximately). The plinth area rateis calculated as $\square 1400$ per sq ft . The future scope stands with scheduling this project and carrying out works of library, auditorium, indoor stadium etc.

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