

**International Journal of Research Publication and Reviews** 

Journal homepage: www.ijrpr.com ISSN 2582-7421

# A Review on- Air Preheater for Spark Ignition Engine for Improving the Efficiency

# <sup>1</sup>Darshan Singh Tomar, <sup>2</sup>Prof. Shamir Daniel, <sup>3</sup>Prof. Amit Khare

<sup>1</sup>M. Tech Scholar, ME Thermal Engineering, Truba Institute of Engineering and Information Technology, Bhopal, Madhya Pradesh, India <sup>2</sup>Assistant Professor, ME Thermal Engineering, Truba Institute of Engineering and Information Technology, Bhopal, Madhya Pradesh, India <sup>3</sup>Assistant Professor, ME Thermal Engineering, Truba Institute of Engineering and Information Technology, Bhopal, Madhya Pradesh, India

## Abstract-

The modern *Spark-Ignition* engine has been in use for a long time and is a reliable power source for countless vehicles around the world. These engines range from simple single-speed two-stroke units found in lawnmowers and portable electric power generators to more complex four-unit found in raceboats and gentle aeroplanes. While petroleum refined from crude oil is now the primary fuel for SI engines, this will not change with the rise of renewable energy and fuels since the engines can run on a broad variety of liquid fuels with little to no adjustment. An air preheater is used to preheat the ambient air by exchanging temperature with the exhaust gas of the engine. This air preheater is like a counter flow heat exchanger which consists of a chamber with an input hole that allows ambient air to be taken inside the chamber and an output hole that sends the preheated air to the carburetor for the combustion process. The SI engine combustion process is characterized by a deflagration that begins at the spark plug site and moves through the combustion chamber. The expansion and combustion phases of the engine provide a number of serious issues, this paper. This paper explained various work that summarize the essential elements of these processes and provide some mathematical methods for describing them in the corresponding working sections.

Keywords-Spark-Ignition; Compression Ignition; Combustion; Spark; Speed.

# 1. Introduction

Both compression-and spark-ignition engines may operate in two- or four-stroke modes. Modern Spark-Ignition (SI) Engines are far more sophisticated than Nikolaus Otto's first in-cylinder compression engine, developed in 1876. The SI engine of nowadays is a proven as well as competent primary mover serving tens of millions of different additional uses in addition to hundreds of millions of passenger automobiles. From very straightforward single-speed two-stroke engines used in lawn mowers and transportable power generators to somewhat sophisticated four-stroke engines used in raceboats as well as small airplanes, these applications span the spectrum. A SI engine currently uses gasoline manufactured from refined crude oil as its main fuel, but this won't make the engine obsolete because it can be modified to run on a number of liquid fuels with minimal to no changes. Gasoline containing up to 10% bio-ethanol may be used without modification in commercially available passenger cars; this entry of microbially substances has just been made permissible in the European Union. This shows how adaptable the fuel is [1-5].

Turbulent premixed combustion is the dominant combustion mode in SI engines, regardless of the fuel used. The combustion process within the cycle takes place over a wide range of pressures and temperatures. The combustion process in gasoline engines is noisy and unpredictable. The power production is directly impacted by the cycle-to-cycle changes in internal cylinder pressure that cause combustion instabilities. Examining these variants can aid with future eradication efforts and improve knowledge of their causes. Achieving improved combustion conditions without adding further disturbances is necessary to increase engine efficiency. Heat loss in the piston and chamber walls and mass flow in gaps such as the top land gap affect combustion. These mass flows can eventually leak some of the charge into the crankcase, reducing efficiency.

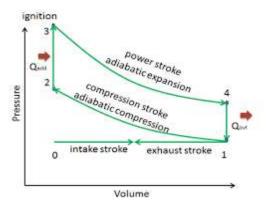


Figure 1-Otto Cycle – pV, Ts Diagram.

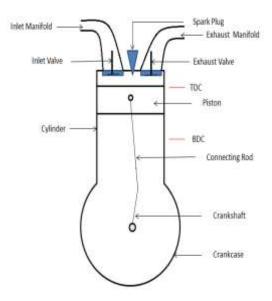
It quickly becomes apparent if one attempts to characterize combustion that it is a pretty complex phenomena in internal combustion engines. A suitable definition would be "unsteady development of extremely exothermic chemical processes in turbulent flow in variable volume non-adiabatic container in the context of mass and heat exchange with the external environment." In addition to these components, a SI engine also has to contain the mechanism of a spark initiating a flame.

Applied engine modeling must therefore find the right balance between the complexity of the mathematical description and the need to continue to make this engine modeling available to designers. This is especially true for so-called parametric studies of engines that require a large number of computers. simulation. Beyond a simple mathematical explanation, the situation is complicated by additional factors such as heat transfer, wave propagation, and the use of combustible fuels in spark-ignited engines [6–10].

Some of these are flame movement, air-fuel mixing, piston movement, heat transfer to and from the combustion chamber, and chemical reactions that release heat. A similar process occurs with the Otto engine.

Spark ignition and four strokes are characteristic of petrol engines. Intake or intake stroke, compression stroke, extension or power stroke, and exhaust are the four different movements. A four-stroke cycle requires the crankshaft to rotate a total of 720 degrees, or 180 degrees on each stroke. As a result, only one mechanical force is generated during the full cycle, as opposed to the crankshaft rotating more than once.

Since the introduction of the internal combustion engine in mobile applications in the late 19th century, it has remained an essential technology for modern road mobility. The internal combustion engine is now the most dependable and cost-effective propulsion system after more than a century of study and technical advancements. Due to its effects on the planet's environment, pollution has become a top focus for engine engineers as a result of the recent sharp decline in air quality. Utilizing alternative fuels is one of several strategies that may be used to solve this issue [11-15].



#### Figure 2-Spark Ignition Engine.

For gasoline engines, hydrogen is thought to be the cleanest alternative fuel. the variety of methods for producing hydrogen and the long-term feasibility of some of those (from fossil fuels, from nuclear power, from renewable energy: biomass, solar, wind, etc.) [2] The numerous energy-generating applications for hydrogen (including gas turbines, fuel cells, as well as internal combustion engines), potential highly efficient, and potentially zero pollution emissions make it particularly enticing.

According to a recent study [3], hydrogen generated by solar or wind energy requires less fuel per hectare of land than other fuels acquired from biomass. Compared to electricity, the use of hydrogen as an energy carrier provides a benefit in terms of volumetric and gravimetric density. Even while hydrogen may be stored in liquefied or gaseous form at high pressures (700 bar), it has a far lower density than the traditional fuels used today, which restricts its autonomy even if it gives greater autonomy than batteries. When comparing the use of hydrogen and the use of hydrogen typically results in greenhouse gas emissions [4]. However, hydrogen has a number of benefits that make it worthwhile to investigate all of its potential applications in spark ignition engines [16-25].

#### 2. Related Work

This section presents various experimental investigations of the *Spark Ignition Engine* fueled. The advantages of using SI are highlighted and the qualitative engine load control strategy is presented by various authors along with the comparative analysis in <u>Table 1</u>.

## 2.1 Several Models on Spark Ignition Engines

It was the focus of (*Sanjay Kumar.D and Srihari., 2018*) study how the intake air temperature affected a SI engine running on diethyl ether-gasoline mixtures. In this research, the effects of diethyl ether (DEE) on the efficiency and emissions of a spark ignition gen-set engine were analyzed. There are three possible DEE/gasoline volume mixes: 3%, 6%, and 9%. An SI four-stroke engine was employed in this investigation. Effects of 32 and 22.1 degrees Celsius intake air temperatures on fuel consumption and emissions were studied. The engine speed is set at 3000 RPM for the test. With a 20% increase in load, the CO level rose to 14 ppm at 22°C and 11 ppm at 32°C, the HC level rose to 260 ppm at 22°C and 140 ppm at 32°C, and the BSFC level rose to 1.10 kg/kWh at 22°C and 1.0 kg/kWh at 32°C. With a 100% increase in load, concentrations of CO, HC, and BSFC all increased by 1 ppm (0.10 ppm at 22°C and 0.08 ppm at 32°C, respectively) at all temperatures.

(*R. Adnan and Z. Sabri Adlan., 2018*) The effect of intake air temperature on the performance of a spark-ignition engine combusting hydrogen peroxide was studied. It is being investigated how the intake air temperature affects the performance of a gasoline engine using a non-traditional fuel. A blend of hydrogen peroxide and ordinary gasoline will be used as an alternate fuel source. While hydrogen peroxide might look like a powerful oxidizer, it really becomes a weak acid when mixed with water. We'll be using a magnetic stirrer to mix everything up. A mixture of 5% hydrogen peroxide by volume (vol) and 95% gasoline (vol) and a mixture of 10% hydrogen peroxide by volume (vol) and 90% gasoline will be used in the experiment (vol). The Precision GX420 single-cylinder, 4-stroke generator engine was employed in the study. The air temperature may be adjusted by a connection between the hot air pistol and the engine inlet. The engine's performance was negatively impacted by the cold air. The experiment showed that, due to increased hydrogen peroxide evaporation at higher temperatures, keeping the engine running at 60 degrees Celsius was more of a challenge than keeping it operating at 40 degrees Celsius.

Authors (*Sumanlal M. R. and Sreeram Nandakumar., 2017*) studied "The Effect of Air Preheating on the Emissions and Performance Characteristics of a DI Diesel Engine Achieving HCCI Mode of Ignition". Examining the effect of diesel vapor induction on engine performance is part of the investigation because it can help researchers achieve homogeneous charge compression ignition (HCCI) or mode of combustion in the engine. Diesel vapor can be produced by utilizing the heat energy of engine exhaust in a Fuel Injection system CI engine by installing a tube and shell exchanger. At full throttle, they measured a number of characteristics of the engine, including its heating value (which would have been 30.05% at room temperature and 41.6% at 65°C), the percentage of carbon monoxide (CO) in the exhaust (0.38% at room temperature but instead 0.28% at 65°C), the percentage of hydrocarbons (HC) in the exhaust (40 PPM at room temperature), and the percentage of nitrogen monoxide (NO), that also increased slightly from 780 to 786 PPM as the temperature goes up.

They conducted an experiment on the "Effect of Inlet Air Preheating on Exhaust Gases in Single Cylinder I.C Engine" by *Madhu L. Kasturi and Amol S. Patil (2017)*. Four-stroke motorcycle engines were tested for the project. By exchanging heat with exhaust gas, they employed an air preheater to warm the input air. On a 2 kilogram weight, the project is tested. They note several outcomes, including an increase in fuel consumption from 550 ml/hr to 560 ml/hr, but decreases in CO and HC levels from 0.11% vol to 0.09% vol and 24% vol to 21% vol, respectively.

(*Bihani Shubham and Kale Sandip., 2017*): "Enhancing the Performance of IC Engine Using Electrolysis and Air Preheater" was the topic of their research. In their project, they employ an air preheater to warm the ambient air utilizing the heat from the exhaust gases that are released by the engine's silencer. This air contains hydrogen gas that was produced by electrolyzing water. The carburetor receives this mixture. Fuel and hydrogen are combined in the warmed air of the carburetor, and this combination is then sent to carry out its intended purpose. The results drawn from the aforementioned experimental and practical analyses are as follows: An increase in the intake air temperature leads to lower fuel usage and greater thermal performance in the brakes. As the temperature of the intake air rises and hydrogen gas is introduced into the combustion chamber, the carbon monoxide level of the exhaust gases somewhat decreases. When compared to HC and CO, oxygen has less negative impacts on human health when the temperature of the intake air rises.

(*Jehad et. al, 2003*) The architect's access to mathematical modeling makes it a powerful tool that not only aids in the creation of new engines but also enables the performance of existing engines to be improved. A computer model of a 4-stroke spark-ignition engine utilizing LPG as a fuel was created with this in mind. Author in this paper discovered that when engine speed (measured in rpm) rises, the combustion time (measured in milliseconds) falls. This is a blatant consequence of turbulence. Better heat transmission between the burnt and unburned zones results from increased turbulence inside the

cylinder as engine speed rises. The combustion time tends to lengthen while running at lean or rich mixes. When traveling at slower speeds, this impact is more pronounced. This is due to the thinner mixture's reduced thermal energy release, which lengthens the ignition delay and delays flame propagation. At lean and rich combinations, the flame temperature is low. Additionally, the incomplete combustion brought on by a lack of oxygen in rich combinations also negatively affects the flame speed. As the compression ratio rises, the combustion duration reduces. Due to a rise in end-of-compression temperature and humidity as well as a decrease in the fraction of leftover gases, the ignition delay shortens when the spark is shifted from the periphery (i.e., XSP = 0.08) to the center (i.e., XSP = 0.5). This is the explanation for this. The limited motion range of the flame is what causes this. Detonation suppression is more strongly influenced by the positioning of the spark. As the combustion duration lengthens, both the burnt and unburned peak temperatures decrease, as does the braking average effective pressure. When the burning period is longer than what is necessary for maximum performance, both CO and NO<sub>x</sub> emissions are reduced. This suggests that the requirements for greatest performance and lowest emissions are not the same.

(*Maher A. R. and others, 2006*) A mathematical simulation model was created to mimic the four-stroke cycle of a spark ignition engine. This modeling model software can be used to study a variety of topics as well as assist in the design of alternative fuel spark ignition engines. The main conclusion of this study is that hydrogen can be used as an additional fuel in modern spark-ignited engines without the need for major modifications, saving large amounts of available petroleum and protecting ecosystems from dangerous pollutants.

Modern spark ignition engines can operate with up to 30% ethanol as a supplemental fuel without requiring significant modifications. Ethanol increases engine output power and lowers NOx emissions when used in conjunction with hydrogen. The presence of hydrogen improves combustion by reducing ignition delay, accelerating flame front propagation, shortening combustion time, and retarding ignition timing, especially in the final stages of combustion. By blending ethanol, peak temperatures, CO and NOx emissions are all reduced. Hydrogen mixture causes a drop in CO concentration but an increase in NOx. The engine power is increased up to a 2% weight ratios of hydrogen fuel and a 30% mass ratio of ethanol fuel. The pace at which heat is released is accelerated by ethanol or hydrogen mixing. Adding hydrogen or ethanol to the fuel lowers both exhaust gas temperature and flow energy.

Ethanol is blended for higher specific fuel consumption, while hydrogen is blended for lower specific fuel consumption. The Reed vapor pressure of the blended fuel increases as ethanol is added, peaks at 10% ethanol addition, and then begins to decline. This indicates an increase in evaporative losses for blended fuels of alcohol and gasoline. The octane rating of blended fuels is increased by blending ethanol with gasoline. Ethanol added at 15% by volume has the same effect on gasoline as lead added at 0.6 g/l or MTBE added at 15% by volume. The vehicle operating zone tends to significantly narrow as the mass ratio of hydrogen to fuel, volumetric efficiency, intake force, and/or intake temperature increase. For spark timing within two to three crank angles of the optimum timing at or close to the stoichiometric equivalency ratio, the operational zone had a retarding possibility. As such, there are practical limits to the performance and efficiency that hydrogen engines can achieve. Due to the lower maximum temperature in the steam generator, the no auto-ignition zone of operation tends to increase when ethanol fuel is present.

(*Jie WanG et. al, 2009*) A spark-ignition engine was numerically simulated to examine the effects of various hydrogen percentages, surplus air ratios, and EGR mass fractions. The estimated and observed incylinder pressure traces and trends in pollutant generation were found to be in good agreement. The outcomes of the simulation demonstrate that NOconcentration grows significantly as hydrogen is supplied and has an exponential connection with temperature. The temperature of the gas and the level of NO in the cylinder are significantly impacted by the introduction of EGR. Even more of a variation in NO concentration will result from the temperature differential. As a result, NO concentration can be successfully reduced by EGR. Regardless of the EGR mass fraction, the NO concentration peaks at the excess air ratio of 1.1.

(Yousef S.H. Najjar et al., 2009) gasoline, liquid fuels, and alcoholic fuels were the three fuel types that were evaluated. In order to assess the performance of a spark ignition engine in various operating scenarios, their properties were integrated to a computer program (design and off-design). It is based on the physical and chemical properties of each fuel and the resulting interactions between the fuel and the engine.

Design service factors of mixing, flammability and knocking, higher compression, advance angle, rotational speed and spark propagation were selected. Performance, especially fuel economy and thermal efficiency, are all components of ultimate performance. Calculations were made the effects of engine speed, spark advance, and equivalence ratio on them were studied. The subsequent conclusions were reached: Iso-octane produces 1.2% higher stopping power than gasoline, 0.5% greater thermal efficiency, and 2.7% less brake specific fuel consumption, bringing them close to parity. Methanol outperforms gasoline in terms of braking force, thermal brake efficiency, and bsfc while using the same amount of energy. While reducing bsfc by 18% and improving thermal efficiency of brakes by 13%, biogas has 10% less braking power than gasoline. The braking power produced by gasoline-hydrogen combination is 7% more than that of regular gasoline. It also exhibits a 2% improvement in brake thermal efficiency and a 5% decrease in brake system friction. Synthetic fuel generates 12% less stopping power than gasoline, 2% less brake thermal efficiency, and 65% more brake system friction.

Spark advance from 0 to 15 degrees BTDC reduces bsfc by 4% while increasing braking power and thermal efficiency by 5%. The braking power and thermal efficiency rise by 2% and 1.5%, respectively, from 15 to 250 BTDC, but the bsfc declines by 1.8%. 15% more braking power is applied each revolution of the engine. At low engine speeds, bsfc is reduced by 1% and thermal braking efficiency is increased by 2%. At high engine speeds, thermal braking efficiency is reduced by 1% and bsfc is increased by 2%.

(*M.V. Mallikarjun et al., 2009*) Author added methanol to gasoline at different ratios and found that adding more methanol produced subtle changes in different subsystems of the engine under different load conditions. gain. In terms of engine performance, the gasoline octane number increased at various methanol blending percentages (0-15%), indicating thermal efficiency and reduced knocking, coupled with improved brake thermal efficiency. However, CO and HC exhaust emissions are significantly reduced, whereas CO2 and Nox emissions are simultaneously marginally rising. It is noteworthy that these methanol mixes have high combustion temperatures and gradually declining exhaust gas temperatures.

(Louis Sileghem et al, 2016) investigated how three test engines modified to run on methanol would perform with greater compression ratios and varied load control techniques applied. Efficiency gains made with methanol are greater than those made with gasoline, and those made with lean combustion and EGR are greater than those made with throttled stoichiometric operation. Turbocharging and a high compression ratio (19.5:1) make it feasible to achieve efficiency that are on par with diesel engines. When lean burn or EGR are used, methanol cuts NOx emissions more significantly.

(J. M. Mantillaet al, 2010) presented a turbulent flame propagation theory-based phenomenological combustion model incorporating research by Keck and colleagues from 1974. In order to use gasoline-ethanol mixtures, the model was modified in accordance with correlations reported by Bayraktar in 2005. The intake valve velocity and combustion efficiency were given new sub-models. These enable modeling of the impact of fuel change, spark timing, and compression ratio. Results are in good accord with both experimental findings in a Cooperative Fuels Research (CFR) engine and those in the original paper.

(*Daniel et. al, 2012*) Using ethanol as a biofuel standard, the authors described the ability of 2,5-dimethylfuran (DMF) to meet biofuel requirements to replace gasoline in spark ignition engines. Particular attention has been paid to how the DMF responds to various engine management settings such as combustion phase (ignition timing), injection timing, relative air/fuel ratio and valve timing (intake and exhaust). The optimization window plays a central role. Using DMF is less sensitive than using gasoline (because of its higher octane rating). The spark retard required to maintain a 2% reduction in peak IMEP at 8.5 bar IMEP was CAD 4.3 for DMF versus CAD 1.5 and CAD 6.6 for petrol and ethanol respectively.

With DMF, this improved ignition delay can reduce isNOx by up to 37% (at 3.5 bar IMEP). These price reductions are consistent with fuel under load. However, ethanol consistently provides the greatest reduction in isNOx emissions (up to 64% at 3.5 bar IMEP) due to less ignition timing sensitivity. DMF shown the lowest sensitivity to VE under different injection timing conditions, whereas ethanol displayed the highest sensitivity since chargecooling had a higher impact on it. When employing DMF, this opens a broader window for emissions optimization. The SOI time window with DMF required 120 CAD to generate a 2-cline IMEP (from max) at 8.5 bar IMEP compared to 90 CAD with ethanol. DMF produced up to 10% lower NOx emissions (similar to gasoline) at modern SOI timings (within this window). AFR was more sensitive when DMF was used than when ethanol was used, and was less sensitive when gasoline was used. At 8.5 bar IMEP, DMF had a lean flammability limit (COV at 5% IMEP) of 1.29, whereas for gasoline this value was 1.24 (and 1.41 for ethanol). Now the claimed efficiency for gasoline is reduced by a small 1.7%, and nothing changes for DMF or ethanol (using DMF increases the declared efficiency by 0.3%). At this 8.5 bar IMEP, the isNOx emission reduction from DMF was even smaller (37%) than gasoline (62%) and ethanol (81%).

The effect of different fuel types on engine performance at different engine speeds has been studied by (*Osama H. Ghazal et al., 2013*). Braking performance, braking torque, and specific fuel consumption were calculated and plotted to show how different types of gasoline affect each scenario considered. A simulation model of a single-cylinder gasoline engine was developed and calculated. Analysis of the data shows that using methanol instead of methane improves performance by about 30% at 1000 rpm and 16% at 6000 rpm. At 1000 or 6000 rpm with the same reference fuel, the increase in consumption is about 100% or 115%. The improvement in thermal braking efficiency at 1000 rpm is about 11% for gasoline and 7% for methanol compared to methane.

(*Victor Pantile et al, 2013*) The authors conducted experiments on a single-cylinder engine with a standard intake system and three valves (one for air, one for hydrogen and one for exhaust). They found that at stoichiometric air-fuel ratios, the effective power produced by hydrogen is approximately 30% greater than gasoline. When using hydrogen, a leaner air/fuel ratio provides effective power equivalent to a gasoline engine. Thanks to improved combustion, fuel consumption during energetic braking is below that of petrol. Using hydrogen in a mixture with an air/fuel ratio of about 1.8 results in higher combustion temperatures and higher NOx emissions. However, as the mixture becomes leaner, NOx emissions decrease dramatically. By changing the relative air-fuel ratio (qualitative control), the NOx emission level is reduced while achieving roughly the same power output as a gasoline engine. The only source of hydrocarbon and carbon dioxide emissions, which are extremely minimal, is the oil burning inside the combustion chamber.

A mathematical model of a dual-fuel four-stroke engine (SI) is provided for comparative study and analysis (*K Rezapour et al., 2014*). It offers the possibility to simulate turbulent combustion and is based on a two-zone combustion model. The model includes cylinder temperature and pressure, heat transfer, brake work, brake thermal and volumetric efficiency, brake torque, brake specific fuel consumption (BSFC), brake mean effective pressure (BMEP), CO2 concentration, brake ratio CO (BSCO) included. predicted., and brake-specific NOx (BSNOx). An analysis of the effects of engine speed, equivalence ratio, and power factor is performed using gasoline and CNG fuels. Natural gas has a lower C/H ratio than gasoline, resulting in lower CO2 and CO emissions. On the other hand, CNG fuel reduces volumetric efficiency, increases combustion temperature and ultimately produces more BSNOx than gasoline. CNG-fueled engines have a lower BSFC than gasoline-fueled engines.

#### 2.2 Emissions in Spark Ignition Engines

(*M. S. Shehata et al, 2008*) An experimental research is conducted to look at engine performance factors and strategies for cutting emissions from spark ignition engines. Air injection rates of 3%, 4%, 5%, and 6% are employed, as well as EGR rates of 5%, 7%, 8%, and 10%. A solution that has promise for enhancing part load operation conditions is the use of EGR in spark ignition engines. With an increase in EGR, the concentrations of BSFC, UHC, CO, and Texhaust rise. Contrarily, with a rise in EGR, braking power, break thermal efficiency, and AFR drop. By raising the temperature of the input charge and reburning UHC and CO, EGR enhances the characteristics of combustion. Increased pumping work caused by higher EGR levels is substantially to blame for decreasing AFR, worsening combustion, and efficiency losses. Some heat is released when the UHC and CO species are

oxidized to CO2 and H2O, contrary to the fact that the exhaust gas increases more after the catalyst than before the catalyst used in the exhaust manifold. significantly reduces UHC and CO concentrations. After opening the exhaust valves used to oxidize UHC and CO to CO2 and H2O at high exhaust temperatures, oxygen concentration increases, so air injection into the exhaust manifold is the easiest way to reduce UHC and CO concentrations is. The increase in AFR at very lean conditions outweighs the heat release effect of the air injection, resulting in a decrease in Texhaust as the air injection mass increases. As engine speed and load increase, the sound pressure level (SPL) also increases. The sound pressure level (SPL) produced with the aid of using the combustion manner is better than the SPL produced with the aid of using the waft manner, and the SPL decided with the aid of using cylinder strain is better than the SPL decided with the aid of using the consumption or exhaust manifold. Engine cycle variation (CCV) is understood to boom with engine pace because of versions in AFR, gas burn rate, warmth launch rate, turbulence intensity, suggest powerful strain, volumetric efficiency, and engine cylinder strain.

(Wojciech Tutak et al 2011) In order to counteract the impacts of air injection's ability to release heat, Texhaust drops as air injection mass increases owing to a rise in AFR to extremely lean circumstances. With an increase in engine speed and load, the sound pressure level (SPL) rises. The SPL estimated from the cylinder pressure is higher than the SPL determined from the intake or exhaust manifold, while the SPL calculated from the combustion process is higher than the SPL produced from the flow process. AFR, fuel burn rate, heat release rate, turbulence intensity, mean effective pressure, volumetric efficiency, and engine cylinder pressure were observed to vary with engine speed, resulting in engine cycle-to-cycle variability (CCV) increases. EGR was very effective in reducing the amount of NO in the exhaust at a given ignition angle, but had a negative effect on other engine characteristics. Engines with exhaust gas recirculation require ignition timing to achieve optimum specifications. However, the amount of NO in the exhaust gas increased as the value of the thermodynamic parameter of the engine thermal cycle increased.

(*Mehrnoosh Dashti et al 2013*) Based on the fundamental rule of thermodynamics, a spark ignition engine cycle simulation has been created. The closed circuits considered in the model, including compression, combustion, ignition delay, and expansion processes, well characterize the thermodynamic processes and chemical states of the working medium. When simulating the combustion process, the two-zone model considered the exhaust gas species CO2, CO, H2O, H2, N2, O2, NO, and UHC. Considerable agreement was found between simulation and experimental results. A parametric study was conducted to examine the effects of equivalence ratio, compression ratio, and ignition timing on engine performance. Such models can be used to deploy alternative fuels or to predict and reduce emissions from conventional fuels for sustainability.

(*Carrie M. Hall et al, 2012*) An engine's ideal CA50 (crankangle at which 50% of the fuel is burnt) is a common measure of combustion efficiency. A flexible 4-cylinder gasoline engine with VVT was further developed and physics-based physics-based experiments were performed to adequately capture CA50 changes due to changes in thermodynamic conditions, valve overlap, spark advance, and over 500 ethanol combo fractions. Tested in paint using the generalizable burn phase version. A factor for the entire operating range of the engine.

In most of these locations (over 90%), the version reasonably predicts gasoline burn rates from SIT to CA50 within 10% of the actual experimental values. Furthermore, it's miles fantastically useful for efforts to manipulate combustion phasing because of its computational simplicity and the reality that it employs simply readings from the engine sensors which can be presently in use. Static look-up tables are often hired in contemporary manipulate strategies to alter ignition, and at the same time as they provide high-quality manipulate for the meant gasoline in regular state, they carry out poorly at some stage in transients and whilst the use of different opportunity fuels. The version defined on this studies can forecast CA50 for severa fuels cycle to cycle, consequently it can be implemented in similarly paintings for remarks manipulate or in a feed ahead predictive manner to beautify manipulate at some stage in transients and whilst the use of opportunity fuels.

Authors Name	Name of Paper	Research Outcome
Yamin, J. A., Gupta, H.	'The effect of combustion duration on the	Due to a rise in end-of-compression temperature
N., & Bansal, B. B. (2003).	performance and emission characteristics of	and humidity as well as a decrease in the fraction
	propane-fueled 4-stroke SI engines'.	of leftover gases, the ignition delay shortens when
		the spark is shifted from the periphery (i.e., XSP =
		0.08) to the center (i.e., XSP = 0.5).
Al-Baghdadi, M. A. S.	'A simulation model for a single cylinder four-	The engine power is increased up to a 2% weight
(2006).	stroke spark ignition engine fueled with	ratios of hydrogen fuel and a 30% mass ratio of
	alternative fuels'.	ethanol fuel.
		The octane rating of blended fuels is increased by
		blending ethanol with gasoline. Ethanol added at
		15% by volume has the same effect on gasoline as
		lead added at 0.6 g/l or MTBE added at 15% by
		volume.
Najjar, Y. S. (2009).	'Alternative fuels for spark ignition engines'.	The subsequent conclusions were reached: Iso-
		octane produces 1.2% higher stopping power than
		gasoline, 0.5% greater thermal efficiency, and
		2.7% less brake specific fuel consumption,
		bringing them close to parity.

Table 1-Comparative	analysis of	existing work.
rubic r comparante	and you of	chioting worth

Mallikarjun, M. V., &	'Experimental study of exhaust emissions &	In terms of engine performance, the gasoline
Mamilla, V. R. (2009).	performance analysis of multi cylinder SI engine	octane number increased at various methanol
	when methanol used as an additive'.	blending percentages (0-15%), indicating thermal
		efficiency and reduced knocking, coupled with
		improved brake thermal efficiency.
Mantilla, J. M., Garzon,	'Combustion model for spark ignition engines	Results are in good accord with both experimental
D. A., & Galeano, C. H.	operating on gasoline-ethanol blends'.	findings in a Cooperative Fuels Research (CFR)
(2010).		engine and those in the original paper.
Daniel, R., Wang, C., Xu,	'Effects of combustion phasing, injection timing,	The spark retard required to maintain a 2%
H., & Tian, G. (2012).	relative air-fuel ratio and variable valve timing on	reduction in peak IMEP at 8.5 bar IMEP was CAD
	SI engine performance and emissions using 2, 5-	4.3 for DMF versus CAD 1.5 and CAD 6.6 for
	dimethylfuran.'	petrol and ethanol respectively.
		At this 8.5 bar IMEP, the isNOx emission
		reduction from DMF was even smaller (37%) than
		gasoline (62%) and ethanol (81%).
Ghazal, O. H. (2013).	'A theoretical study of the SI engine performance	At 1000 or 6000 rpm with the same reference fuel,
	operating with different fuels'.	the increase in consumption is about 100% or
		115%. The improvement in thermal braking
		efficiency at 1000 rpm is about 11% for gasoline
		and 7% for methanol compared to methane.

# 3. Ignition Processes

Internal combustion engines required spark ignition (SI) or compression ignition (CI) to ignite the mixture (CI). Before the introduction of dependable electrical technologies, hot tube and frame techniques were employed. A laser-ignited research engine was created.

#### 3.1 Spark Ignition Process

The ignition system of a gasoline engine is typically powered by an alternator or a mixture of a dynamo as well as a lead-acid battery. The battery supplies both start-up and shut-down power. In addition, the battery delivers electrical energy when the alternator cannot sustain voltages beyond 13.8 volts (for a typical 12V automotive electrical system). The lead-acid batteries takes a greater percentage of the electrical demand when the generator voltage falls below 13.8 volts. The alternator produces primary power underneath practically all running circumstances, including regular idling. While the throttle is wide open, certain systems deactivate electricity in the alternator field (rotor). By turning off the field, the mechanical load on the alternator pulley is reduced to near zero, increasing crankshaft performance. In this situation, the battery provides all of the primary electrical energy. A gasoline engine sucks in a combination of air and gasoline and compresses it to 12.8 bar (1.28 MPa).

As the piston reaches the cylinder head and maximum stroke, a spark plug ignites the mixture as it compresses. An induction coil or transformer supplies the requisite high voltage (often 10,000 volts to over 30,000 volts). An induction coil is a flyback system that interrupts the principal system current with a form of synchronous circuit breaker. Contacts or power transistors serve as breakers. Capacitive discharge ignition systems are used in several ignition systems. A step-up transformer is used in the CD ignition.

A step-up transformer generates an electrical spark by using the energy stored in a capacitor. A mechanical or electrical control mechanism in each system provides precisely timed high voltage to the proper cylinders. Through the spark plugs, this spark ignites the air-fuel combination in the engine's cylinders. Although gasoline internal combustion engines are considerably simpler to start in cold weather than diesel engines, they might have issues starting in very cold weather. For many years, the answer was to park in a warmed space. In certain regions of the world, the oil was emptied, heated overnight, and then reintroduced into the engine for a hard freeze.

In the early 1950s, gasoline carburetor units were invented, and in cold weather, naphtha was routed into the unit, where some of the fuel was burnt and the remaining was converted into superheated liquid and fed straight to the intake valve manifold. This item was widely used until electric engine block warmers became standard equipment for gasoline engines sold in cold locations (*Gurram, A. M., 2016*).

# 3.2 Diesel Ignition Process

For ignition, diesel and homogeneous compression ignition (HCCI) engines rely only on the heat and pressure generated by the engine during the compression phase. The compress number is generally double that of a gasoline engine. A diesel engine consumes just air and injects a little quantity of diesel fuel into the cylinder right before optimum efficiency, igniting the fuel instantaneously. Due to high pressure and heat, HCCI-type motors use both air and fuel yet rely on unaided self-combustion.

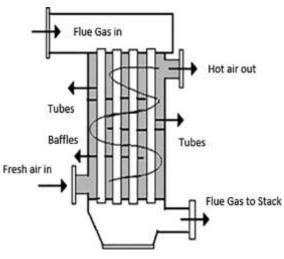
This is also why Diesel and his HCCI engines have cold start issues. Glow plugs are used in light indirect injection diesel engines in vehicles and light trucks to warm the combustion chamber soon before starting to prevent dead starts in cold weather. A battery and charging system are also standard on

most diesel engines. Nonetheless, this system is secondary in that it starts the engine, switches the fuel on and off (which can alternatively be done with a switch or mechanical mechanism), and operates various electrical components and accessories. The manufacturer includes it as a premium item to facilitate The majority of modern engines rely on electric and electronic engine control units (ECUs) to manage the combustion process and boost efficiency while lowering pollutants (*Bansal, B. B., 2003*).

# 4. Air Pre-Heater

When starting a process that requires hot air, such as combustion in a boiler furnace, it is common practice to first heat the air to a higher temperature. These heat exchangers are often employed in power plants to improve boiler efficiency. In order to turn the water within the boiler into steam, coal is burned in the furnace, releasing a great deal of heat that is then used to boil the water. In order for the coal particles inside the furnace to catch fire, a minimum ignition temperature and the stoichiometrically needed amount of air must be present in the right proportions and be well mixed together. The introduction of air-pre heaters helps to save fuel by reducing the amount of energy needed to heat the air before the coal can catch fire within the furnace. Air-preheaters have several drawbacks that must be considered.

APH may be broken down into two major groups: restorative and regenerative. In a recuperative system, the hot fluid is constantly losing heat to the cold fluid. Both tube-style and grill air-pre heaters may be found here (APHs). The heat transfer between the warm and cold liquids in a regenerative system is also not continuous. Two types of air preheating systems fall under this category: RAPH (rotating-plate air preheating) and APH (fixed-plate air preheating). Since these heat exchangers are so widely used in industry, we will be focusing on regenerative air-pre heaters. A number of drawbacks are also connected to using an air-preheater. Recuperative APH is further subdivided into tube and plate-type APH, while regenerative APH is split into revolving plate APH and stationary plate APH.



#### Figure 3-Air-Preheater.

An air-preheater is a type of heat exchanger that allows heat to be transferred from a hot fluid to cold air. Doing so allows one to lessen the amount of energy needed to warm the air-fuel mixture. By heating the intake air in advance, it may be possible to completely burn up the surplus fuel. Heat exchangers come in many shapes and sizes, with a variety of flow patterns. The concentric tube or twin pipe heat exchanger is perhaps the simplest. One pipe is nested inside another in a heat exchanger with twin pipes. Both fluids have their own dedicated inlet and output ducts [21].

The primary function of a preheater is to warm up the asphalt that has been salvaged in preparation for the subsequent recycling process. The preheater is easily portable and may be towed by a tractor at high speeds. As it does its job, the preheater may drive itself slowly and steadily. In order to swiftly switch between locations, the preheater has to be very mobile. Setup and breakdown time combined shouldn't exceed half an hour. The self-driving system must be able to function within a specific speed range and accept unlimited speed changes within that range in order to facilitate the recycling process.

# 5. Objective

The following can be accomplished by the installation of an air preheating system in a gasoline engine:

- To lower fuel consumption.
- To Fuel cost savings.
- To release less pollutants when the engine is running.

#### 6. Conclusion

Internal combustion engines employ two completely distinct mechanical mechanisms for ignition: spark and compression. However, the compression ignition (CI) and spark ignition (SI) engines, which use different spark ignition technologies, work in certain ways similarly and share the same operating principles. It is clear from the study above that several experimental techniques have been used to increase the efficiency of spark ignition engines. In addition to this, a significant amount of research has been conducted utilizing simulation tools to assist forecast the impact of different factors on engine performance. The studies conducted demonstrate the potential of simulation tools for application in spark ignition engines' complicated combustion, emission, and efficiency analyses.

#### References

- 1. Gurram, A. M. (2016). Studies on Spark Ignition Engine-A Review.
- Aleonte, M., Cosgarea, R., Jelenschi, L., & Cofaru, C. (2011). Technical solutions for improving the efficiency of a two stroke SI engine. Bulletin of the Transilvania University of Brasov. Engineering Sciences. Series I, 4(2), 1.
- Aina, T. O. P. E., Folayan, C. O., & Pam, G. Y. (2012). Influence of compression ratio on the performance characteristics of a spark ignition engine. Advances in Applied Science Research, 3(4), 1915-1922.
- Shehata, M. S., & Abdelrazek, S. M. (2008). Engine performance parameters and emission reduction methods for spark ignition engine. *Engineering Research Journal*, 120, M32-M57.
- 5. Tutak, W. (2011). Possibility to reduce knock combustion by EGR in the SI test engine. Journal of KONES, 18, 485-492.
- Dashti, M., Hamidi, A. A., & Mozafari, A. A. (2017). Study of Performance and Environmental Emissions of a Gasoline Spark Ignition Engine. Int. J. Sustain. Futur. Hum. Secur, 1(1), 8-14.
- Hall, C. M., Shaver, G. M., Chauvin, J., & Petit, N. (2012, June). Combustion phasing model for control of a gasoline-ethanol fueled SI engine with variable valve timing. In 2012 American Control Conference (ACC) (pp. 1271-1277). IEEE.
- 8. Ge, H. W., Juneja, H., Shi, Y., Yang, S., & Reitz, R. D. (2010). A two-zone multigrid model for si engine combustion simulation using detailed chemistry. *Journal of Combustion*, 2010.
- 9. Murthy, P. V. K. (2012). Combustion modelling in a two-stroke copper coated spark ignition engine. *The Experiment*, 3(1).
- 10. Pandey, K. M. (2012). CFD analysis of intake valve for port petrol injection SI engine. *Global Journals of Research in Engineering*, *12*(A5), 13-19.
- 11. Sridhar, K., Murali, R. B. V., Younus, S. M., & Lakshmi, K. M. (2013). Computerised Simulation of Spark Ignition Internal Combustion Engine. *IOSR J. Mech. Civil Eng*, 05-14p.
- Chaudhari, A. J., Sahoo, N., & Kulkarni, V. (2014). Simulation models for spark ignition engine: a comparative performance study. *Energy Proceedia*, 54, 330-341.
- 13. Tatschl, R., Pötsch, C., Priesching, P., Schuemie, H., Vitek, O., & Macek, J. (2014, April). A scalable simulation methodology for assessment of SI-engine performance and fuel consumption on component, subsystem and system level. In *Transport Research Arena (TRA) 5th Conference: Transport Solutions from Research to DeploymentEuropean CommissionConference of European Directors of Roads (CEDR) European Road Transport Research Advisory Council (ERTRAC) WATERBORNE<sup>TP</sup>European Rail Research Advisory Council (ERRAC) Institut Francais des Sciences et Technologies des Transports, de l'Aménagement et des Réseaux (IFSTTAR) Ministère de l'Écologie, du Développement Durable et de l'Énergie.*
- 14. Rezapour, K., Mason, B. A., Wood, A. S., & Ebrahimi, K. M. (2014). Bi-fuel SI engine model for analysis and optimization.
- Pantile, V., Pana, C., & Negurescu, N. (2013). Improvement of the Performance of a Spark Ignition Engine by using Hydrogen. UPB Sci. Bull., Series D, 75(3), 111-120.
- 16. Ghazal, O. H. (2013). A theoretical study of the SI engine performance operating with different fuels. *International Journal of Mechanical and Mechatronics Engineering*, 7(12), 2526-2529.
- Daniel, R., Wang, C., Xu, H., & Tian, G. (2012). Effects of combustion phasing, injection timing, relative air-fuel ratio and variable valve timing on SI engine performance and emissions using 2, 5-dimethylfuran. SAE International Journal of Fuels and Lubricants, 5(2), 855-866.
- 18. Mantilla, J. M., Garzon, D. A., & Galeano, C. H. (2010). Combustion model for spark ignition engines operating on gasoline-ethanol blends. *Revista de Engenharia Térmica*, 9(1-2), 89-97.

- Sileghem, L., & Van De Ginste, M. (2011, June). Methanol as a fuel for modern spark-ignition engines: efficiency study. In *Proceedings RUG-FTW Ph. D. Symposium*. Amsterdam, The Netherlands: Elsevier.
- Mallikarjun, M. V., & Mamilla, V. R. (2009). Experimental study of exhaust emissions & performance analysis of multi cylinder SI engine when methanol used as an additive. *International Journal of Electronic Engineering Research*, 1(3), 201-212.
- 21. Najjar, Y. S. (2009). Alternative fuels for spark ignition engines. The Open Fuels & Energy Science Journal, 2(1).
- Wang, J., Huang, Z., Liu, B., & Wang, X. (2009). Simulation of combustion in spark-ignition engine fuelled with natural gas-hydrogen blends combined with EGR. Frontiers of Energy and Power Engineering in China, 3(2), 204-211.
- Al-Baghdadi, M. A. S. (2006). A simulation model for a single cylinder four-stroke spark ignition engine fueled with alternative fuels. *Turkish Journal of Engineering and Environmental Sciences*, 30(6), 331-350.
- Yamin, J. A., Gupta, H. N., & Bansal, B. B. (2003). The effect of combustion duration on the performance and emission characteristics of propane-fueled 4-stroke SI engines. *Emirates Journal for Engineering Research*, 8(1), 1-14.
- 25. Verhelst, S. (2000). Simulation of the combustion of alternative fuels in spark ignition engines. In *Proceedings First RUG-FTW Ph. D. Symposium.*
- Srihari, S., Kumar, D. S., & Thirumalini, S. (2018). Effect of inlet air temperature on SI engine fueled with diethyl ether-gasoline blends. *Journal of Mechanical Engineering and Sciences*, 12(4), 4044-4055.
- Adnan, R., Adlan, Z. S., Munir, F., & Asnawi, M. (2006). Experimental study on the effect of intake air temperature on the performance of spark ignition engine fueled with hydrogen peroxide. *Stroke*, 2000, 66.
- Sumanlal, M. R., Nandakumar, S., & Mohanan, P. (2017). The Effect of Air Preheating on the performance and emission characteristics of a DI Diesel Engine achieving HCCI mode of combustion. *International Journal of Theoretical and Applied Mechanics*, 12(3), 411-421.
- Kasturi, M. L., Patil, A. S., Shinde, N. P., & Jagtap, P. R. (2017). Effect of inlet air preheating on exhaust gases in single cylinder IC engine. *International Research Journal of Engineering and Technology*, 4(7), 55-58.
- Sandip, K., Shubham, B., Mandar, B., Suraj, B., & Anil, D. (2017). Enhancing the Performance of IC Engine using Electrolysis and Air Preheater. *International Journal of Engineering and Management Research (IJEMR)*, 7(3), 469-473.