



Influence of Gating System for Electrical Panel Part Component by Simulation Flow Analysis using NX-Easy Fill Advanced Software

Srinivasa G.¹, L.G. Sannamani², Dr. S. N. Ravi Shankar³

¹Student, M. Tech, Tool Engineering, GT&TC, Mysuru-16, Karnataka, INDIA

²Deputy General Manager, GT&TC, Mysuru-16, Karnataka, INDIA

³Principal, Post Graduate Studies, GT&TC, Mysuru-16, Karnataka, INDIA

ABSTRACT

With the increasingly short life span on wide range of consumer electronic products, the manufacturing process of injection moulding remains- the most popular method for producing plastic components for assembly. The feed system in injection moulding is made up of sprue, runner systems, and gates, which are the channels through which the polymer flows. In the manufacturing of plastic parts the process requires a molten polymer being injected into a cavity inside a mould, which is cooled and later ejecting the part. The main phases in an injection moulding process therefore involve filling, cooling and ejection. The cost-efficiency of the process is dependent on the time spent in the moulding cycle. Die design is the most time consuming stage, hence, Mould flow is used to analyze die design and for testing mould flow result, comparison have been done with experimental design.. The present work focuses on the impact of an ideal gate location on melt front time and defects using NX-Easy Fill Advanced software through number of iterations. The new optimized gate position was tested in an injection moulding machine with a developed mould. Software tools were developed to evaluate possible energy consumption and environmental impact among different process plans. Estimation based on nominal conditions can lead to underestimation due to changing conditions of machining. By the software support, more reliable estimation was achieved with considering various operational parameters and conditions.

Keywords: Injection moulding, mould flow, NXEasy Fill Advanced software.

1. INTRODUCTION

Injection moulding is a manufacturing technique for making different complex parts from both thermoplastic and thermosetting plastics materials in the production. Molten plastic is injected at high pressure into a mould, which is the inverse of the product's shape. After a product is designed, usually by an industrial designer or an engineer, moulds are made by a mould maker (or toolmaker) from metal, usually either steel or aluminum, and precision machined to form the features of the desired part. Injection moulding is widely used for manufacturing a variety of polymer parts, from the smallest component to entire body panels of cars. Injection moulding is the most common method of production, with some commonly made items including bottle caps and outdoor furniture.

2. OBJECTIVES

- Component study and development.
- One whole shot was designed and analyzed.
- Injection mould calculation and conceptual design.
- To manufacture a component that is free of fundamental flaw

3. METHODOLOGY

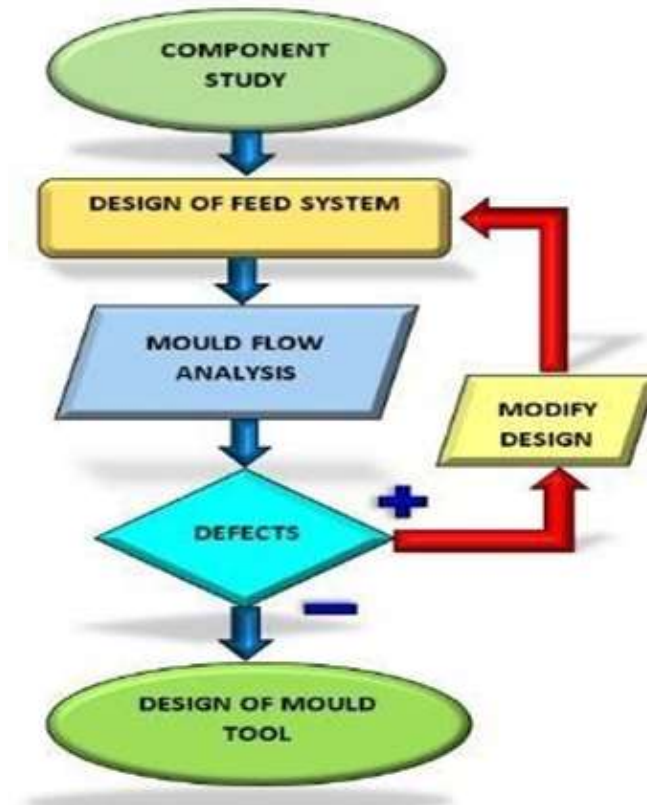


Fig.1–Flow chart of Methodology

3.1 Component study

The component name is electrical panel part which is used as the component of electronic board/ Panel Board. The component is black in color. To make the component of the desired color, black masterbatch is used. The component's volume is 21.97cm^3 . The total weight of the components is 19.72 g. The component has a density of 0.898 g/cc and has reduced by 0.8 % of its original volume. The melting point is 160°C . The component's 3D model is shown in Fig.2

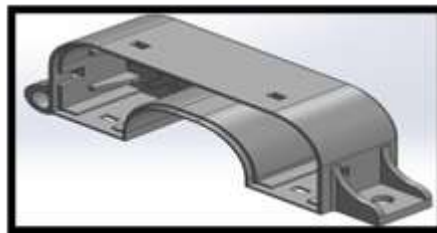


Fig.2 -Top Case Electrical Panel Part

Design of Feed System

3.2.1 Sprue design

A standard sprue design is chosen and modified for its diameter based on the diameter of the runner at one end, and the other end dimension is obtained from the relationship.

$$D1 = D2 + 2L \tan(A)$$

Where,

$D2$ = Diameter of sprue at lower end,

$D1$ = Diameter of sprue at upper end i.e., 3.5 mm end,

SH or L = length of sprue selected by the designer = 80.86 mm and

$A = \text{tapered angle } (1 - 5^\circ) = 1.25^\circ \text{ (taken)}$

$$D_1 = D_2 + 2L \tan A$$

$$D_1 = 3.5 + 2(80.86) \times \tan(1.25^\circ) = 7.03$$

Hence, the diameter of sprue is 7.03 mm which is rounded off to 7 mm

3.2.2 Runner design

$$\frac{\sqrt[3]{L}}{3.7} \times \sqrt{w}$$

Where,

$w = \text{weight of the component, } g = 19.72g$

$L_r = \text{length of the runner} = 9.83$

$L_r \cong 10$

$$\text{Diameter of runner } (\phi) = \frac{\sqrt[4]{10}}{3.7} \times \sqrt[3]{19.72}$$

Diameter of runner $(\phi) = 2.15 \text{ mm}$

For ease of machining and ease of cutter availability it is rounded off to 3 mm

3.2.1 Gate Width

Width of the gate (W_g) is calculated by:

$$W_g = \frac{n \times \sqrt{A}}{30}$$

Where,

n is the material constant,

for Poly Propylene $n = 0.8$

$$W_g = \frac{0.8 \times \sqrt{21251.52}}{30}$$

$W_g = 3.89 \text{ mm} = 4 \text{ mm}$

3.2.3 Gate height (h)

$$h = n \times t$$

where,

$n = 0.8$

$t = \text{Avg. wall thickness} = 1.76 \text{ mm}$

$$h = 0.8 \times 1.76$$

$$h = 1.41 \text{ mm} = 1 \text{ mm}$$

3.2.3 Gate length (l)

$$L = h + (W_g/2)$$

$$L = 1.408 + (3.89/2)$$

$$L = 3.25 \text{ mm} = 3 \text{ mm}$$

Therefore, the gate's thickness is 1 mm. Because the part is made for a single impression mould and has a rectangular profile, one can only create a nedge gate for feeding. In two-plate mould fabrication, a nedge gate is used. The edge gate must have been thin and be able to bend in order to de-gate. Typical gate thickness range from 1-1.5 mm, while sizes for glass reinforced materials may be greater.

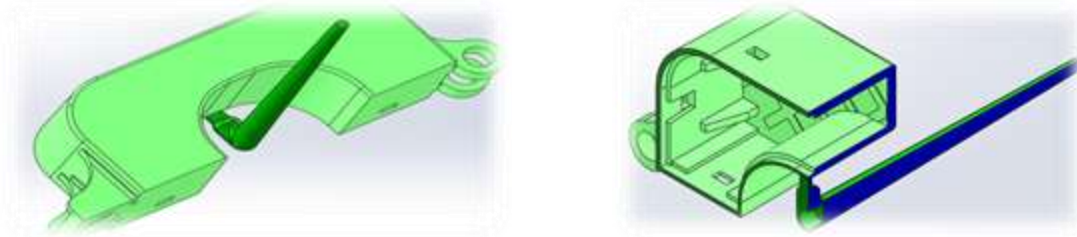


Fig.3-Edge gate and feeding system design

Mouldflow Analysis

Mould flow analysis is a study of plastic material flow that aims in the evaluation of the part, parameters, and mould design in order to produce high-quality parts. Mouldex 3D program controls NX Easy-Fill Analysis. It's an integrated mould flow simulation tool that lets designers test the mouldability of plastic part designs early on in the product development process. Developers can also make adjustments ahead of time to improve gate /locations, material selection, part design, process conditions, or selection of materials.

Table 1 Input data for analysis

Supplier	Advance composites'
Trade name	ADX2017
Material selected	PolyPropylene
Density	0.898g/cc
Melt Temperature	160 °C
Mold Temperature	50 °C

NX Easy Fill Advanced Results

The mould flow simulation is run several times, and the top two gate iterations are displayed, with the best one being chosen for manufacturing based on gate contribution, fill time, pressure and air traps.

1. Edge Gate Flow Analysis Results

The time taken by the polymer to completely fill the core and cavity is referred to as fill time. It is essential to determine how quickly the polymer is injected into the mould. In the first iteration depicted in Fig 4, the part filling is unbalanced and fills in 2.97 s with a pressure of 6.31 MPa, and at a temperature of 205.01 °C. If the fill pressure is too high or too low, defects such as mould flashing appear, affecting the component's surface quality. From the Fig. 4(d) it is clear that pressure is high while filling the cavity and core. The blue region or dots visible in Fig 4(e) are areas where air has been entrapped as a result of air being not able to escape through the vents or inserts given in the mould. Weld lines are caused by the material used, as well as the design and structure of the component. They happen when polymer flows from opposite directions contact at the same area. The red lines visible in Fig. 4(f) indicate weld lines formation in the component. Furthermore, ejection is problematic because 1 mm gates shred/tear the component surface due to shear stress induced by ejector pins.

Table 2 Results from Edge Gate Analysis

Sl. No.	PARAMETERS	RESULTS
1	Gate contribution	Unbalanced flow
2	Melt front time	2.98s
3	Pressure	6.310MPa
4	Temperature	205.01 °C
5	Air traps	Less
6	Weld lines	Less
7	Ejection	Difficult/Complex

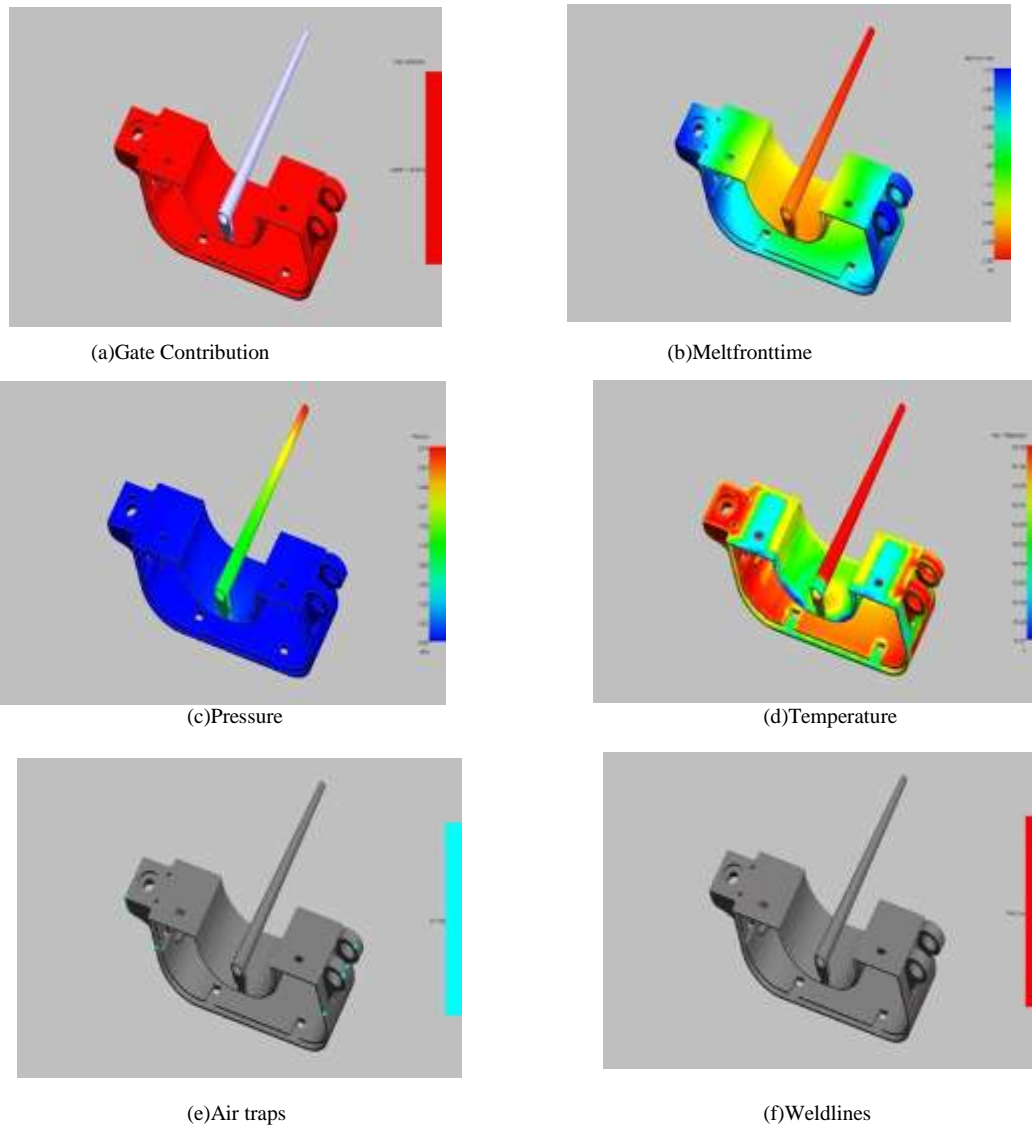


Fig.4 FlowsimulationwithEdgeGatesfor(a)Gate Contribution(b)Meltfronttime (c)Pressure (d)Temperature (e)Air traps (f)Weldlines.

2. SubmarineorTonnelgateFlow AnalysisResults

Since the edge gate results were unsatisfactory, the feeding system was modified to submarine gate or tonnel gate, 0.5 mm diameter of upper end, and 7 mm diameter of lower end, and length 16.50 mm as illustrated in Fig.5, where the portion fills in 1.50 with a pressure of 8.50 MPa, with some negligible air traps but marginally lower weld lines than previous results. Ejection is very easy in submarine gate compared to edge gate.

Table 3 Results from Tonnel gate Flow Analysis Results

Sl.No.	PARAMETERS	RESULTS
1	Gate contribution	Unbalanced flow
2	Melt front time	1.500 s
3	Pressure	8.50 MPa
4	Temperature	205.02 °C
5	Air traps	Minimum
6	Weld lines	Minimum
7	Ejection	Easy (Autodegate)

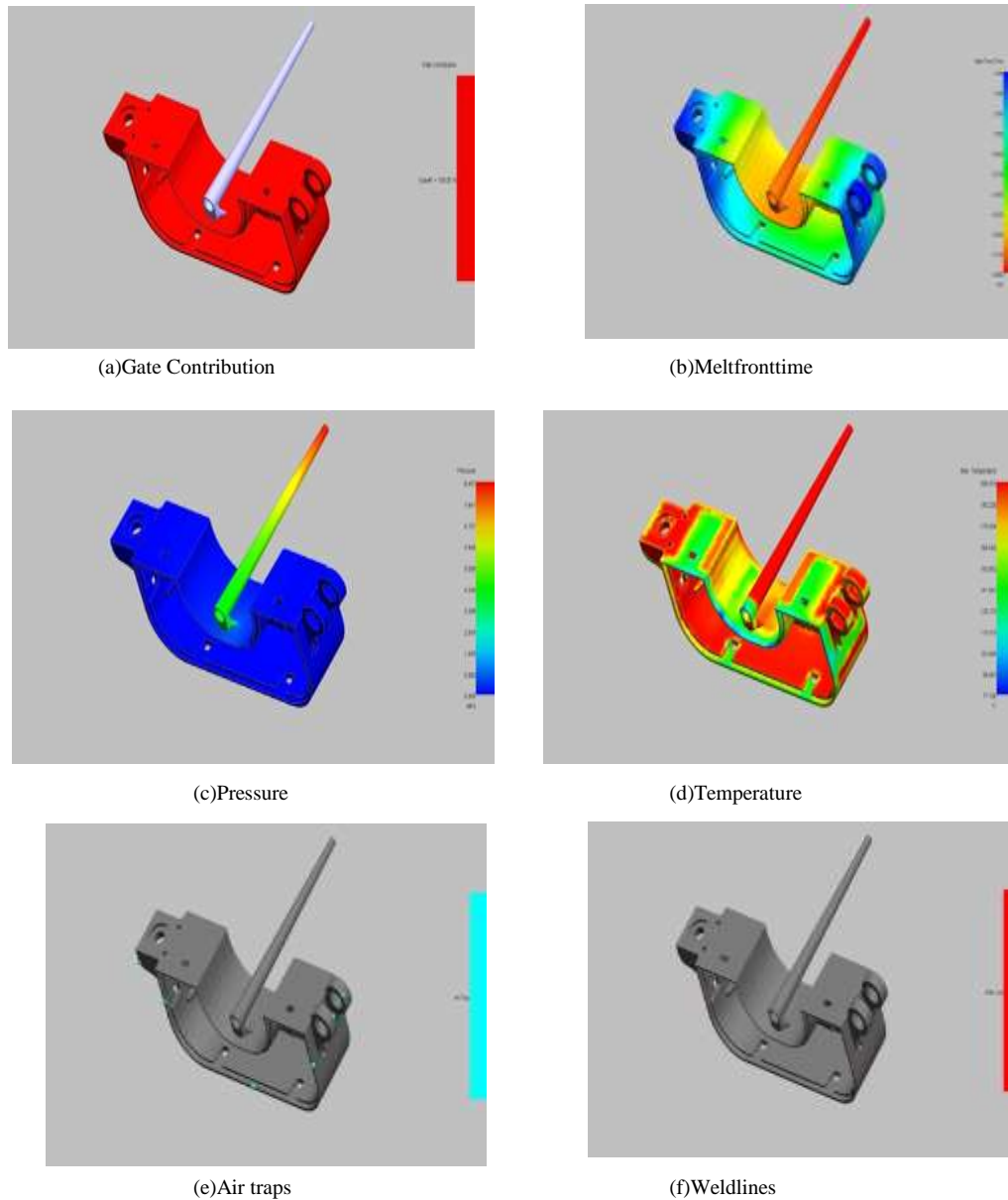


Fig.5 Flowsimulation with submarine gates for (a) Gate Contribution (b) Melt front time (c) Pressure (d) Temperature (e) Air traps (f) Weld line

CONCLUSIONS

The analysis for optimum gate and runner location was explained, and flaws such as air traps and weld lines were eliminated in the flow simulation by comparing the above two results. Automatic de-gating is achievable because the gate is placed in the ideal location for easy production and defect-free components. By including air vents in the core and cavity inserts, air traps can be reduced. Weldlines can be regulated by checking up on injection pressure, barrel velocity, and mould temperature. From the Table 4 edge gate and submarine gate points result has been approved for further manufacturing process.

Table 4 Comparison of two iteration results

Sl. No.	PARAMETERS	EDGE GATE POINTS	SUBMARINE GATE POINTS
1	Gate contribution	Unbalanced Flow	Slightly Unbalanced
2	Mouldability	Good	Very Good
3	Melt front time	2.98s	1.50 s
4	Pressure	14.23MPa	8.50MPa
5	Temperature flow	205.01 °C	205.02 °C
6	Air traps	Minimum	Minimum
7	Weldlines	Less	Acceptable

8	Ejection	MoreDifficult&Complex	Easy(AutoDe-gate)
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References

- [1]. "A Study on Two Plate and Three Plate Mold of Ultra Thin Plates in Minimizing Warpage Issue", M. Fathullah1, Z. Shayfull1, S. Sharif2, N. A. Shuaib1 and S.M. Nasir1 | November 2011
- [2]. "Effect of Heat Treatment Processes on the Mechanical Properties of Medium Carbon Steel", T. Senthil Kumar1,* and T. K. Ajiboye2 revised January 2012
- [3]. "Effect of Different Laser Types on Material Engraving Process", Kadhim A. Hubeatir1*, Mohammed MAL-Kafaji2 and Hadeel J. Omran2, Published: 06/11/2018
- [4]. "Effect of Varying Gate Size on the Air Traps in Injection Molding", Arjun Kapila†*, Kanwarjeet Singh†, Gaurav Arora† and Narayan Agarwal† Vol.5, No.1 (Feb 2015)
- [5]. "Material Selection For High Performance Moulds", Vasco, J. I., Capela, C. I., Bártolo, P. I., Granja, D. 2 November 2007
- [6]. "Analysis of rubber bush mould Using Mould-Flow and compare with experimental result", H. H. Makwana1, October 2015
- [7]. "Spark Analysis Based on the CNN-GRU Model for WEDM Process", Changhong Liu1,2, Xingxin Yang3, Shaohu Peng3, Yongjun Zhang1,*, Lingxi Peng2 and Ray Y. Zhong4. Published: 16 June 2021
- [8]. "Software Support for Environmentally Benign Mold Making Process and Operations", aeyoung Kong, Seungchoun Choi, and David Dornfeld October 2011
- [9]. "Analysis and Design of Multi Impression Split Core, Finger Cam Operated Mold For Brass Insert Connector Plug", Lokeswar Patnaik, Sunil Kumar, 5th to 8th April 2017
- [10]. "Design and Simulation of Plastic Injection Moulding Process", Wong, C. T., Shamsuddin Sulaiman, Napsiah Ismail & A. M. S. Hamouda, January 200.
- [11]. Vikas B. J1, Chandra Kumar R2, "Influence of feeding system in injection moulding for lower washer of a bearing", International Journal of Research in Engineering and Technology. Volume: 02 Issue: 08 | Aug-2013.
- [12]. Thanusha Nandish1*, L. G. Sannamani2, "The influence of gate location in a vertical injection moulding part connecting plate", International Research Journal of Engineering and Technology, Volume: 07 Issue: 05 | May 2020.