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## **Appraisal of Strength Characteristics of Bituminous additive Lateritic Soil as Pavement Material in construction industry**

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### **ABSTRACT**

This research investigated the bituminous additive prerequisite of some lateritic soil samples as pavement materials. Both chemical and geotechnical experiment were carried out on untreated (raw) and improved laterite. Bituminous material was utilized in the present research as admixture. The California bearing ratio (CBR), Atterberg limit (Liquid and plastic limit), specific gravity, moisture content, and compaction experiments of the samples were performed with varying percentages or proportions of bitumen; 3, 6, 9 and 12%. The soil categorization test reveals that the lateritic soil is between A-2-7 and A-2-4 which is silty or clayed clayey gravel and sand based on AASHTO soil categorization. The C.B.R values are 9.87, 4.35% and 7.28% for samples A, B and C correspondently at 0% additive content, while for 12% additives, the result showed maximum C.B.R values for sample A and B as 41.21% and Sample C as 40.04%. Thus, bitumen has been verified to be a good admixture on the enhancement of the properties of lateritic soil as pavement materials.

Keywords: Strength Characteristics, Bitumen, Lateritic Soil, pavement materials.

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### **1.0 INTRODUCTION**

Majority of available soils are deficient in some vital engineering properties to carry the anticipated superimposed loads, thus enhancements have to be performed to make these soils better by means of soil stabilization or /enhancement (Oluwatuyi et al. 2018; Shalabi et al. 2017). Lateritic soils can be defined as groups of soils that have a broad variety of yellow, red, and brown, fine-grained soils of light or weightless texture plus cemented soils, and nodular gravels (Adeyanju and Okeke 2019a). Abundance or copiousness of these soils and their promising structural and geotechnical properties make them valuable as a construction foundation or pavements material for low-cost building or housing, highways or express roads, airfields, and compacted fill in earth embankments (Adeyanju and Okeke 2019b; Ogiye et al. 2018; Yoobanpot et al. 2017; Hassan et al. 2016). Akinje (2015) illustrate soil stabilization or improvement as the treatment of raw soil to enhance its engineering properties. Stabilization aimed at adding inert materials and enhancing the soil density so as to increase the ostensible cohesion and small friction resistance materials (Mengue et al. 2017; Akinwumi, 2014). Chemical soil enhancement using Portland cement to stabilize the soil through replacement and compaction technique with rolling equipment revealed the cured outcome as a low-grade concrete (Al-Homidy et al. 2017; Akinwumi et al., 2012). Similarly, bitumen is a genetic or chromosomal name for numerous mixtures of semisolid or solid (Osinubi and Amadi 2010), hydrocarbons gaseous, liquid in nature, as well as totally soluble in carbon disulphide (Adeyanju and Okeke 2019b; Latifi et al. 2013). The most popular materials within genus of bitumen are asphalts, tars, and pitches. They have tendency to remain at solid surface and its adhesiveness is subject to the surface scenario and the state of the bitumen (Adeyanju and Okeke 2019b).

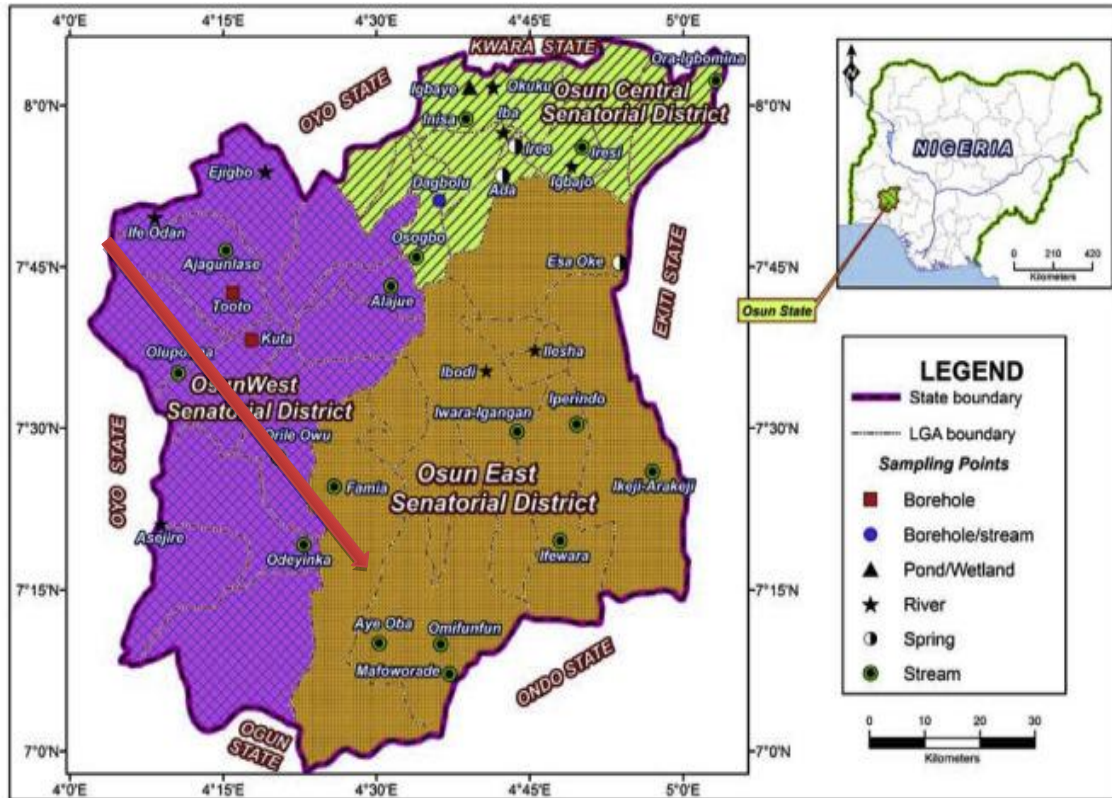


Fig. 1: Map of study area, Osogbo Osun state (Google 2021).

## 2.0 MATERIALS AND METHODS

The Lateritic soil was obtained from three distinct site located at KM 10 Osogbo – Ibadan Highway, Osun State, Nigeria as displayed in Figure 1. Ongoing highway construction works exposed the soil layers and the samples were taken at 2m depths from the natural ground surface via Trial Pit techniques. The sampling was air dried so as to tackle the aggregating capabilities of lateritic soils upon exposure to air as asserted by Abe (2019). The Portland cement used for this experiment was purchased from the Osogbo market, whereas S 125 bitumen utilized was obtained from Dekit Construction Company in Osogbo, Osun State, Nigeria (Coordinates 7.7827°N, 4.5418°E). Experimental Engineering strength tests on treated and untreated samples were performed in the laboratory of Civil Engineering Department, Federal Polytechnic Ado-Ekiti, Ekiti State, Nigeria in accordance with AASHTO (American Association of State and Transportation Officials), 2007 recommendation for 0, 3, 6, 9 and 12% additive.

Table 1: Outcomes of Preliminary experiments

Features	Soil Samples Description		
	A	B	C
Particle Size Distribution			
Fine (%)	90.86	93.46	93.91
Coarse (%)	09.16	06.56	06.11
Bulk density (KN/m <sup>3</sup> )	14.63-29.75	12.24-22.23	14.63-22.77
Consistency Test (%)			
Liquid Limit (LL)	43.02	43.51	21.51
Plastic Limit (PL)	19.08	25.66	16.34
Plasticity Index (PI)	23.92	17.86	5.18
Specific Gravity	2.70	2.71	2.69
Group index	19.01	19.02	18.88
Optimum moisture content (%)	9.16	9.91	9.16
Maximum Dry Density (Mg/m <sup>3</sup> ) 1.325	1.866	1.663	1.481
CBR (%)	9.89	7.28	4.37
AASHTO Classification	A-2-7	A-2-7	A-2-4
Soil Category	Silty or clayed clayey gravel and sand		

### 3.0 RESULTS AND DISCUSSION

#### A. Outcomes of Preliminary Experiments

Results of preliminary experiments on the three lateritic soil are displayed in Table 1. It demonstrated that the soil is categorized as A-2-7 and A-2-4 based on AASHTO classification method. This infer that it below the suggested standard for pavement construction work, thus it require enhancement.

#### B Outcomes of Oxide Composition of Cement and Bitumen

Results of the oxide composition of cement and S125 bitumen are demonstrated in Table 2. The result displays the main chemical constituents of cement which are CaO, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, MgO etc.

This illustrates that cement is a good pozzolana that may assist further stimulation of the formation of other hydration reaction products such as lime, rice husk ash and/or fly ash. Though bitumen shows less water penetration and adding cohesion strength in appearance because bitumen stabilization comprises of cementation and water proofing deeds.

Table 2: Results of Oxide Composition of Portland cement

Cement		Bitumen		
Features	Composition (%)	Features	Values (%)	Test Standard
CaO	66.32	Form	Thick viscose liquid	Obvious
SO <sub>3</sub>	1.13	Colour density g/m <sup>3</sup>	Dark Brown	Obvious
SiO <sub>2</sub>	20.04	Solid content %		
MgO	1.06	Penetration @25.2 <sup>o</sup> C	40+- 5	ASTM D5
Fe <sub>2</sub> O <sub>3</sub>	3.74	Service Temperature C <sup>o</sup>	1.04+-0.01	ASTM D2939
Na <sub>2</sub> O	0.28	Setting time (hours)		
Insoluble residue	0.13		6.01 – 47.01	ASTM D2939
Al <sub>2</sub> O <sub>3</sub>	5.93			
K <sub>2</sub> O	0.64		8 touch dry – 24 x firm set	ASTM D2939
LOI	0.07			

#### C. Outcomes of Atterberg Characteristics

The test results are displayed in Figures 2- 5. It reveal that the cement additive (3%) Liquid limit and plastic limit value is greater than bitumen additive, while bitumen additive (3%) plasticity index (PI) higher than cement additive. Meanwhile at 12% bitumen additive, plasticity index higher than cement additive. This decline in liquid limit for the mixing proportions of Portland cement, and S125 bitumen, can be as a result of the pores in the lateritic soil, that filled up by the particles of the two stabilizers or improvers and minimize vulnerable with rising water content which is in agreement with Grazi et al. 2017.

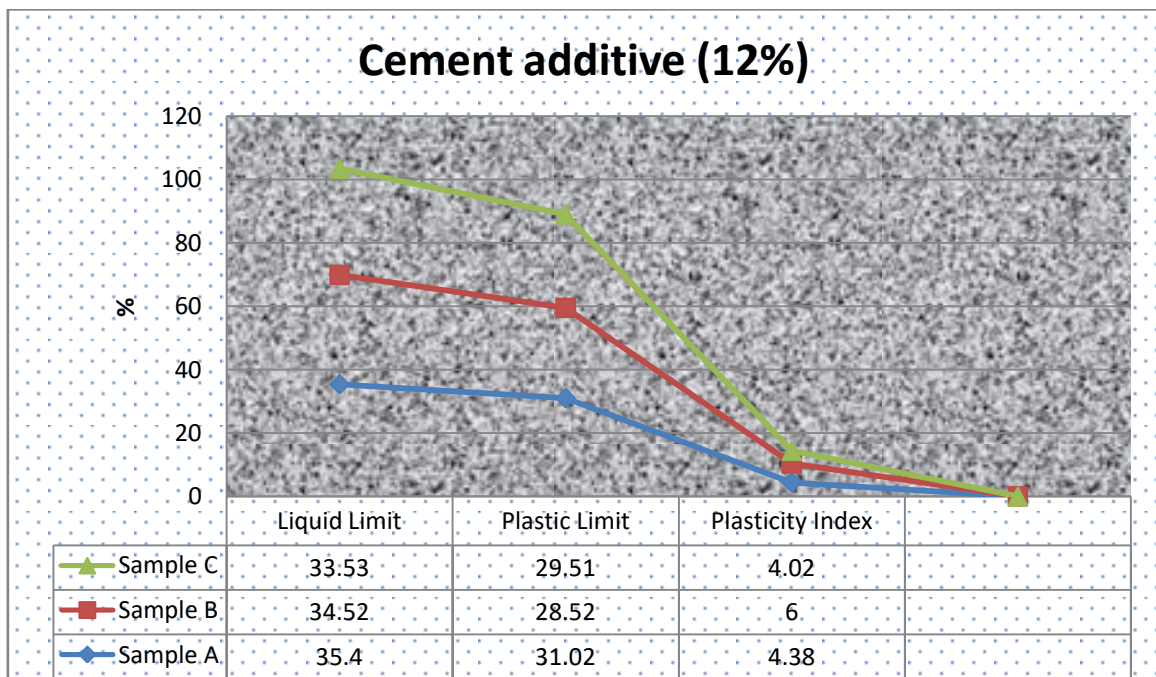


Fig. 2: Atterberg Limit test for cement additive at 12%

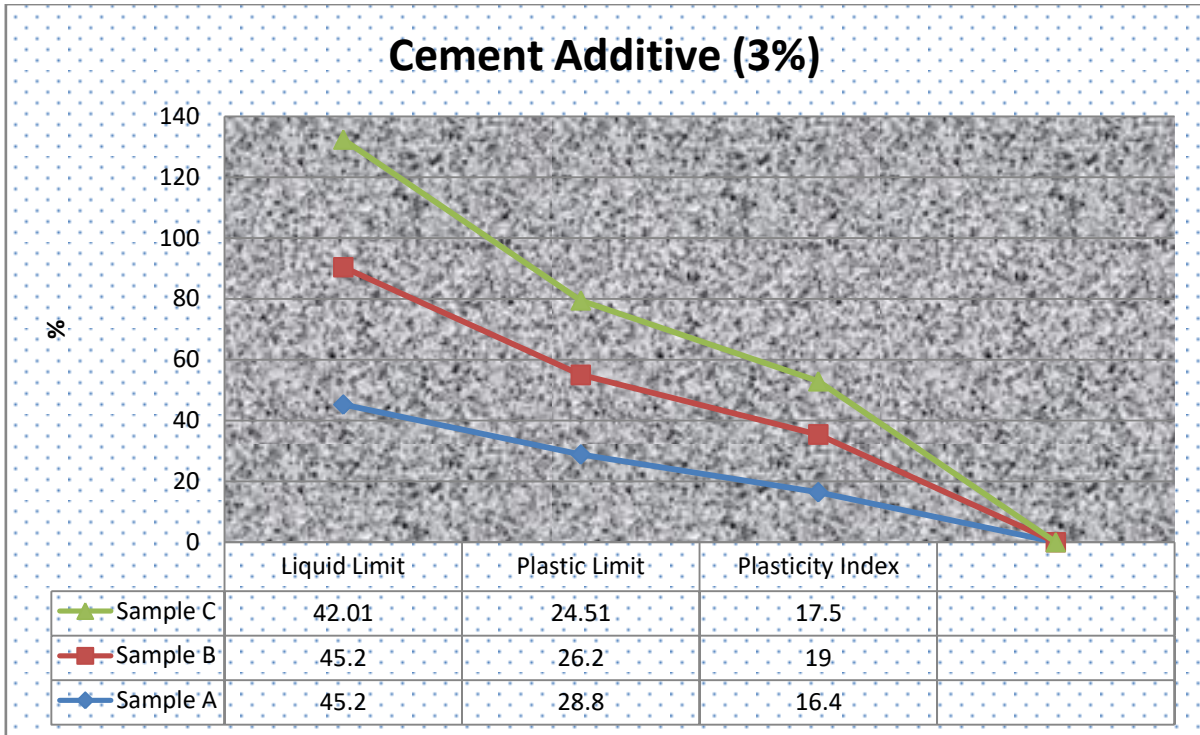


Fig. 3: Atterberg Limit test for cement additive at 3%.

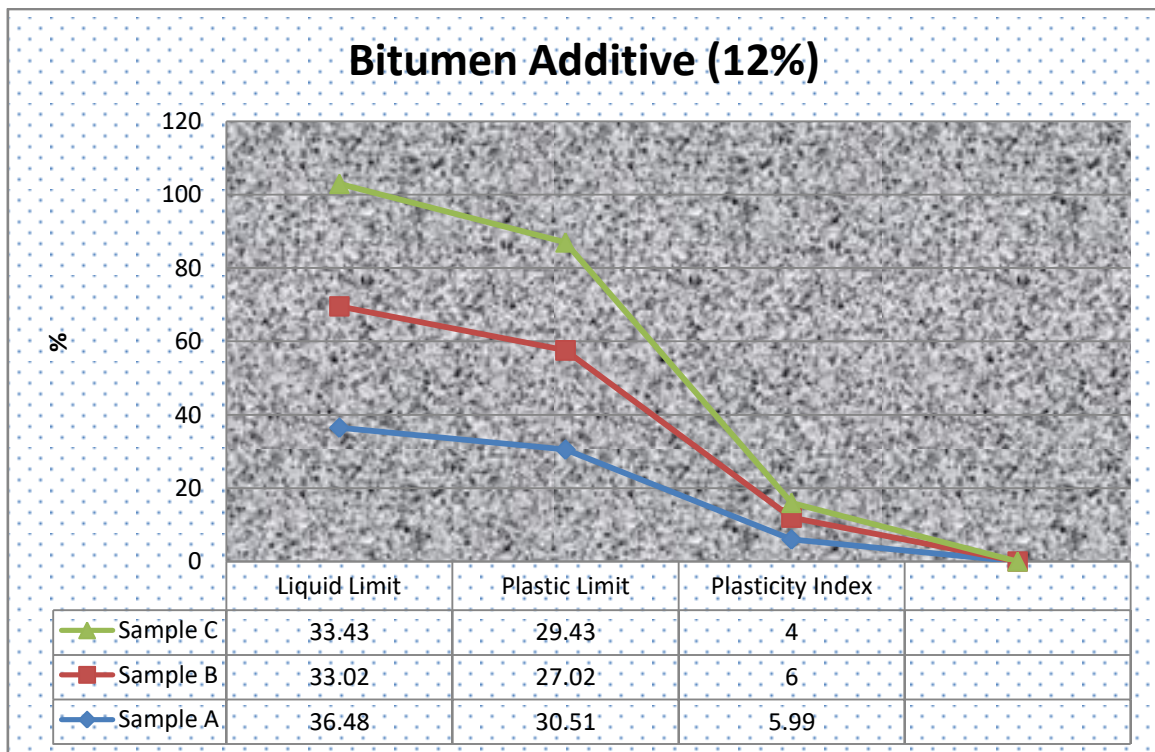


Fig. 4: Atterberg Limit test for bitumen additive at 12%

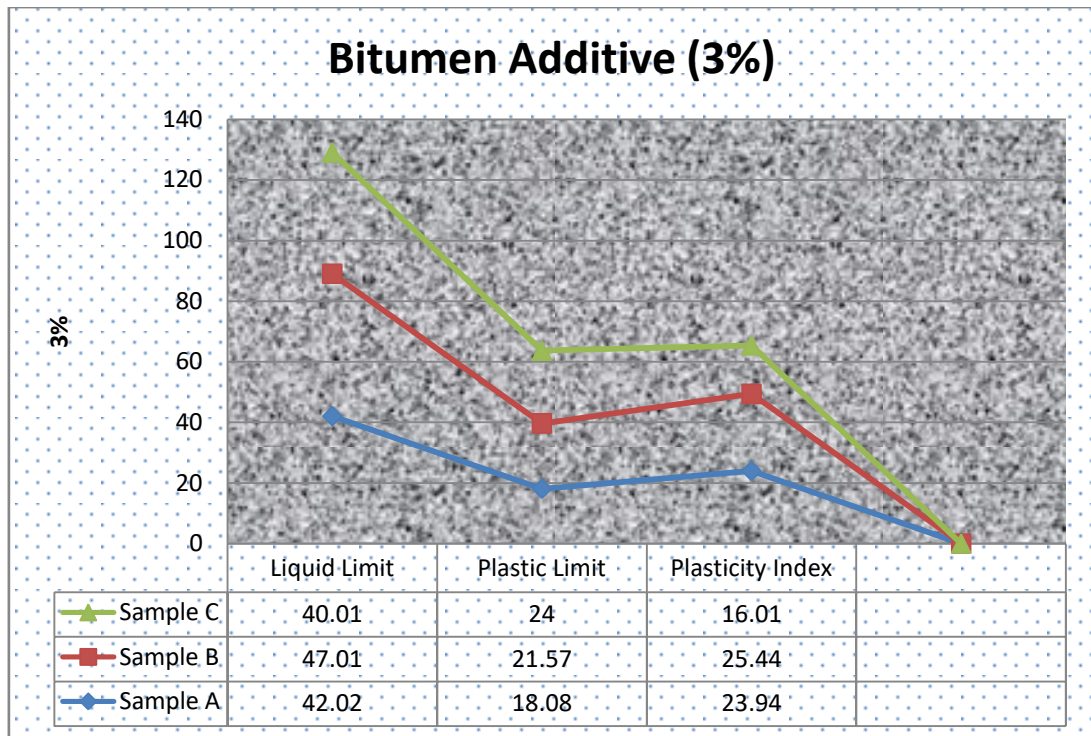


Fig. 5: Atterberg Limit test for bitumen additive at 3%.

*D. Outcomes of Compaction Characteristics*

Figures 6-9 demonstrated the variations between OMC (Optimum Moisture Content), MDD (Maximum Dry Density) with S125 bitumen addition. The MDD improved with increase in S125 bitumen content. The values range from 1.866mg/m<sup>3</sup> at 0% to 2.003mg/m<sup>3</sup> at 10% S125 bitumen content. Similarly, OMC diminishes from 9.91% at 0% to 7.04% at 12% S125 bitumen. The increasing of mixing ratios might cause by flocculation and accumulation of fine-grained soil particles which filled up the available larger space before improvement and consequently resulted to a corresponding fall in dry density. Grazi et al. (2017) and Adeyanju and Okeke(2019b) reported similar results.

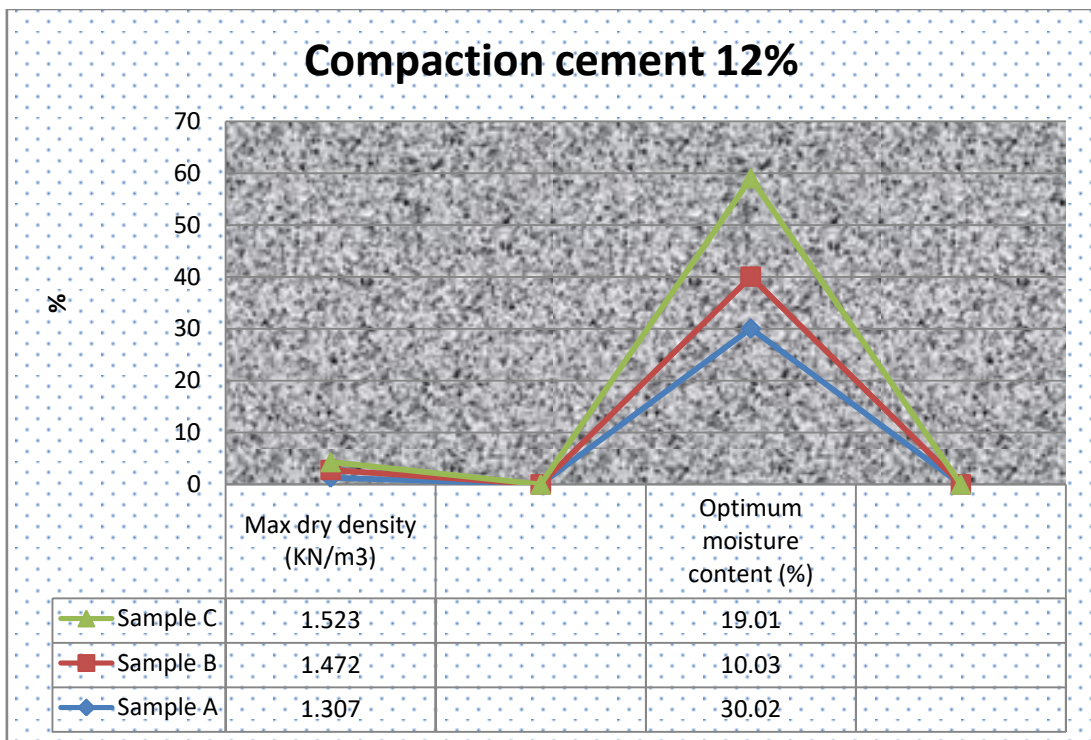


Fig. 6: Compaction characteristic for cement additive at 12%.



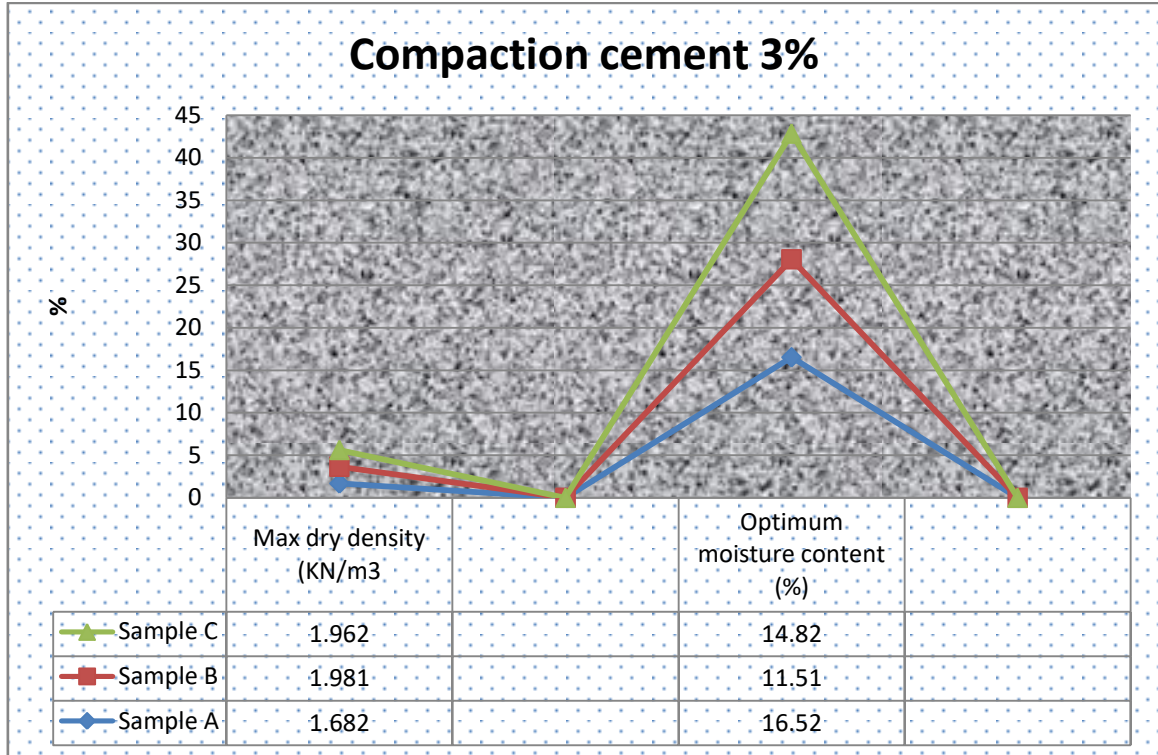


Fig. 7: Compaction characteristic for cement additive at 3%.

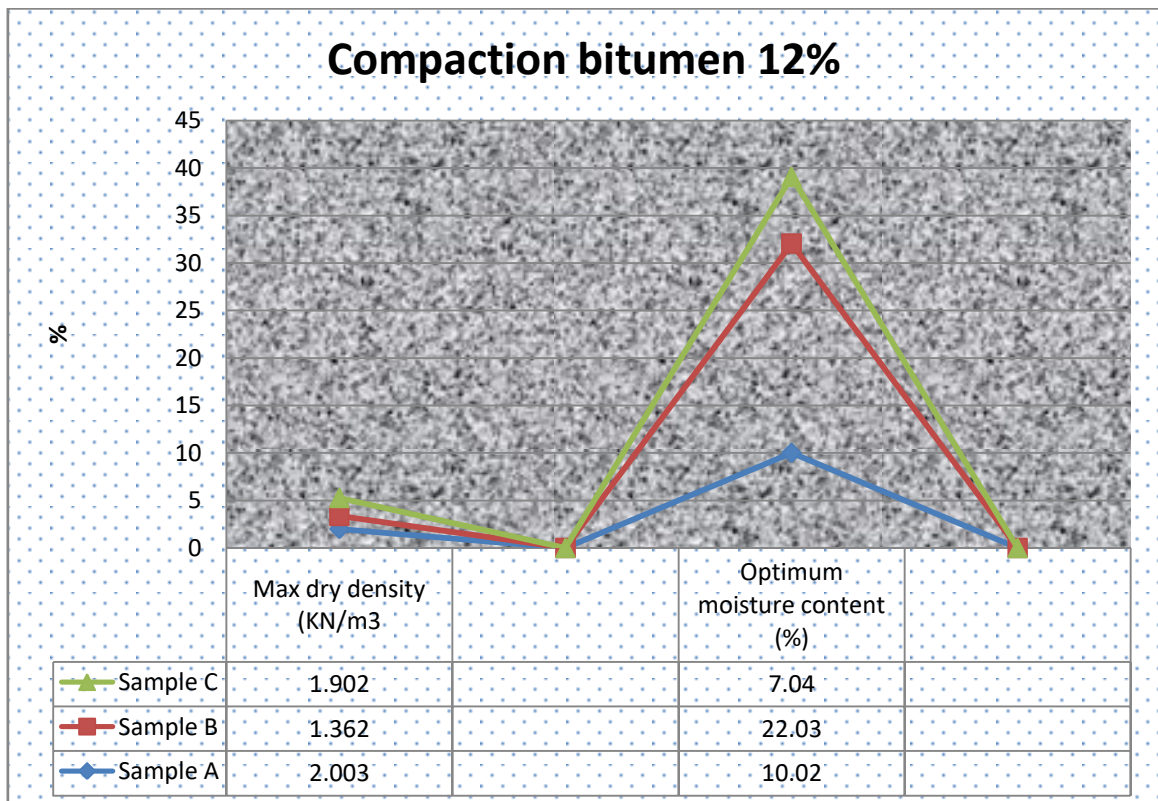


Fig. 8: Compaction characteristic for bitumen additive at 12%.

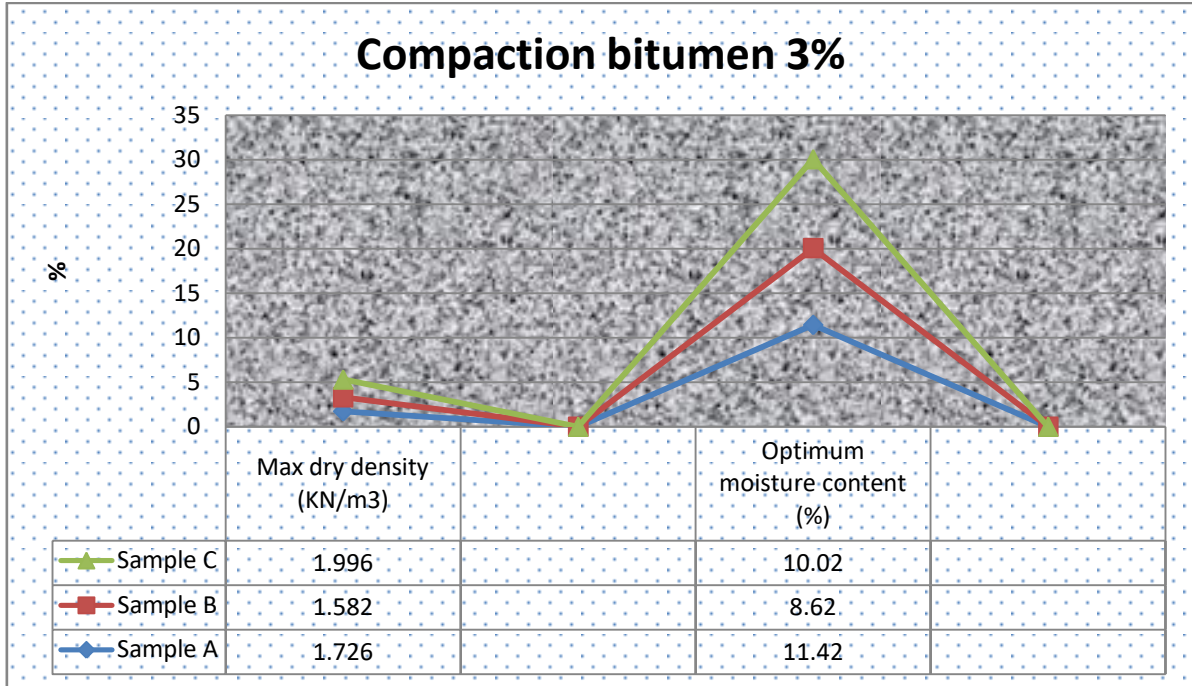


Fig. 9: Compaction characteristic for bitumen additive at 3%.

*E. Outcomes of California Bearing Ratio (CBR)*

From Table 1 AASHTO 2007 characterized the threesamples as bad pavement materials due to their lowdry densities and strength, thus improvement is required. Outcomes of CBR test is displayed in Figures 10 & 11. The results revealed that CBR values amplified from 9.89% at natural (raw) soil level to 41.02% at 12% bitumen content, which is below cement additive of 55.02% at 12%.

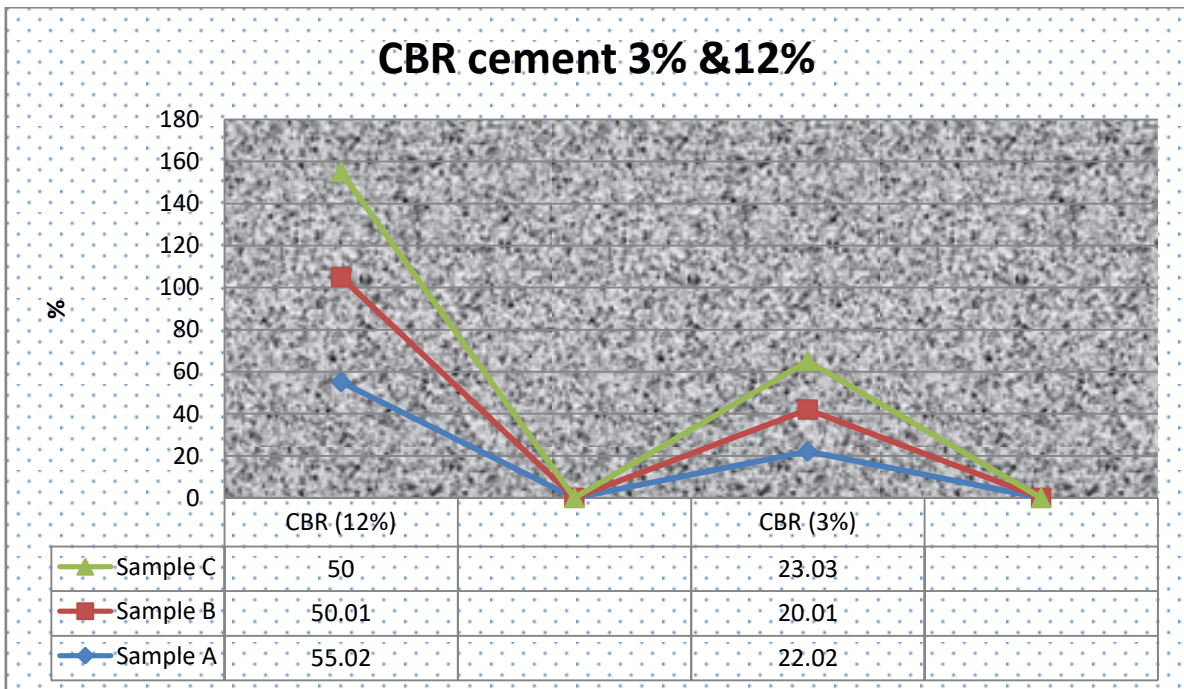


Fig. \10: CBR characteristic for cement additive at 3% and 12%

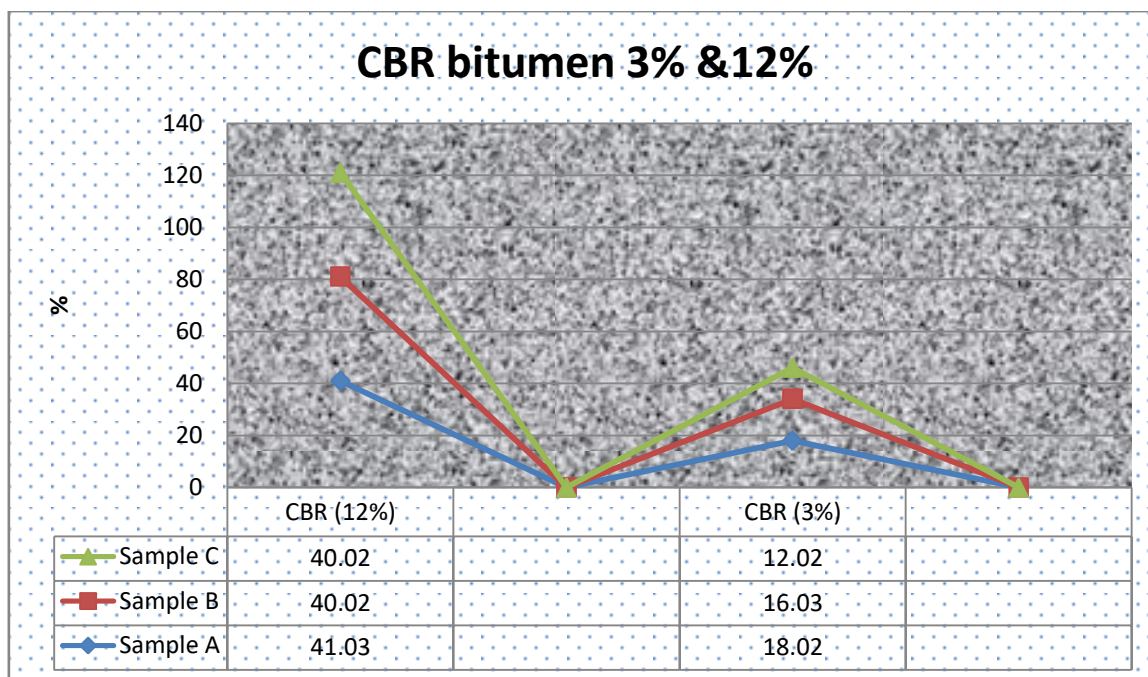


Fig. 11: CBR characteristic for bitumen additive at 3% and 12%

## CONCLUSION

The following conclusions were made on the basis of the investigations:

- Categorization test shown that the lateritic soil was grouped as A-2-7 and A-2-4 soil, that is Silty or clayed clayey gravel and sand.
- At 6% Portland cement content (PCC), the experiment displayed a general improvement in MDD with 3% S125 bitumen content. Whereas, OMC also diminished with increase in S125 bitumen content.
- It was identified that CBR increased with 3% bitumen content for the 6% cement content.
- Thus, bitumen is confirmed or inveterate to be a beneficial admixture in lateritic soil enhancement using 6% cement and 3% bitumen.

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